

Design And Analysis Of Scramjet Inlet

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ABSTRACT: SCRAMJET or Supersonic Combustion Ramjet Engine is an air breathing engine, which has no rotating parts. It is similar to ramjet engine except the combustion chamber having supersonic flow and the operating Mach number is from 6 to 8. In scramjet, flow is supersonic throughout the engine. Unlike turbojet they don't have stages of blades, so they are lighter. They have a major advantage over rockets that they don't have to carry oxidizers onboard which further decrease their mass and increase their specific impulse. The problem statement of this paper is the design of the inlet of scramjet with the maximization of the static pressure at air inlet exit.

KEYWORDS: CFD Analysis, Inlet Modeling, Ramps, Scramjet Inlet

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I. INTRODUCTION:

The definition of ramjet is important to understand the definition of scramjet engine; scramjet is the successor of ramjet. Ramjet's do not have any rotating parts, instead work on the principle of compression of supersonic air to low speed i.e. to subsonic speed and therefore leads to increment in static temperature and static pressure and then fuel is injected to initiate combustion, and finally flow is accelerated to supersonic speed through nozzle. Because of deceleration Mach number, the rise in temperature, density, pressure at the entrance of combustion chamber are high. Near about 6 Mach, and due to this it becomes difficult to slow down the speed to subsonic. So when the speed is not reduced to subsonic, but to desirable supersonic speed, then ramjet becomes scramjet.

Scramjet depends on vehicle speed to compress the incoming air and decelerate it before entering the burner (ramjet), but in scramjet engine the flow remains supersonic throughout the entire engine, whereas in ramjet the flow velocity is reduced to subsonic, so scramjet can work effectively at greater speeds.

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II. SCRAMJET INLET:

Air intake or inlet is the primary module of the aero-engine and plays a very vital role, as it is responsible for capturing the air from surrounding and transferring to the combustion chamber for combustion process without much loss, hence the engine-intake capability is necessary while considering design. As the air mass flow rate depends on the efficiency of air intake, it is necessary to design inlet with proper geometry and accurate manufacturing to achieve better engine performance.

Scramjet inlet achieves compression through introduction of ramps which produces series of oblique shock waves, causing increase in static pressure and temperature of the flow and reducing Mach number. Due to nature of design of scramjet engine, it operates at hypersonic speed and hence in this case inlets are called as diffusers. Here compression is achieved by both external and internal compression. So internal compression inlet is the longest and the heaviest and as the name suggests, the compression takes place internally. The other type of inlet is external inlet, where compression occurs externally and has no starting requirements and is the shortest. Third type of inlet is mixed compression inlet where both internal and external compression takes place, it's longer hence heavier and also requires, more cooling for hypersonic speed.

III. DESIGNING THE INLET:

- **STEP 1 – Theoretical Analysis**

Calculation of rise in static pressure, static temperature, density after introduction of ramps in air inlet using formulas:

$$M_{n,1} = M_1 \sin \beta$$

$$M_{n,2}^2 = \frac{1 + [(\gamma - 1)/2]M_{n,1}^2}{\gamma M_{n,1}^2 - (\gamma - 1)/2}$$

$$\frac{\rho_2}{\rho_1} = \frac{(\gamma + 1)M_{n,1}^2}{2 + (\gamma - 1)M_{n,1}^2}$$

$$\frac{p_2}{p_1} = 1 + \frac{2\gamma}{\gamma + 1}(M_{n,1}^2 - 1)$$

$$\frac{T_2}{T_1} = \frac{p_2}{p_1} \frac{\rho_1}{\rho_2}$$

$$M_2 = \frac{M_{n,2}}{\sin(\beta - \theta)}$$

• STEP 2 – Calculation of Inlet Dimensions

Inlet length, ramp height area ratio is being calculated using formulas:

$$h_n = \frac{A_n}{A_2} (h_2)$$

Where A is the area and,

$$\frac{A_n}{A_2} = h_n d_n / h_2 d_2$$

$$d_2 = d_n$$

$$\frac{A_n}{A_2} = \frac{h_n}{h_2}$$

A_n/A_2 = area ratio after each oblique shock, and $h = 0.152m$

❖ Now to calculate the height of ramps for the first three shocks are :

$$x_0 = h_0 \tan(\beta_1)$$

Where β_1 = wave angle

And h_0 = height of engine inlet

Now, the length of fourth shock can be found out by using the formula:

$$x_1 = h_0 / \sin \delta$$

δ = Ramp angle

So, combining and x_0 and x_1 we will get the total length of the inlet.

• STEP 3 – Modeling in CATIA

After the calculation of all the dimensions, inlet was modeled using CATIA, and all the models are shown below. For all the models cowl angle is 0 degrees.

• Step 4 – CFD Analysis

Analysis is being done on fluent 18.1(student version) and SSTK-OMEGA model has been used.

IV. THEORETICAL VALUES FOR VARIOUS MODELS:

For analysis purpose various models were being considered and values of static pressure was calculated and from those models three models based on the values of static pressure at exit was selected for CFD analysis. The results are tabled below.

S.No	Number of ramps used	Ramp Angles	Mach number at entrance of inlet	Mach number at exit of inlet	Static Pressure (pa)
1	2	9.1, 8.5	8	5.1249	16,418.05
2	3	9.5,9.6,12.6	8	5.964	91,858.81
3	3	9.5,9.6,14	8	4.698	1,19,691
4	3	5.5,11.8,15.1	8	4.354	19,228,9821
5	4	6.5,7.6,9,13.5	8	2.572	64,744.48
6	4	5.69,8.5,10.8,13.1	8	3.505	1,59,844.40
7	4	5.69,8.5,10.8,13.1	5	3.4785	37,081.75

Inlet Model(For Above Three Selected Models)

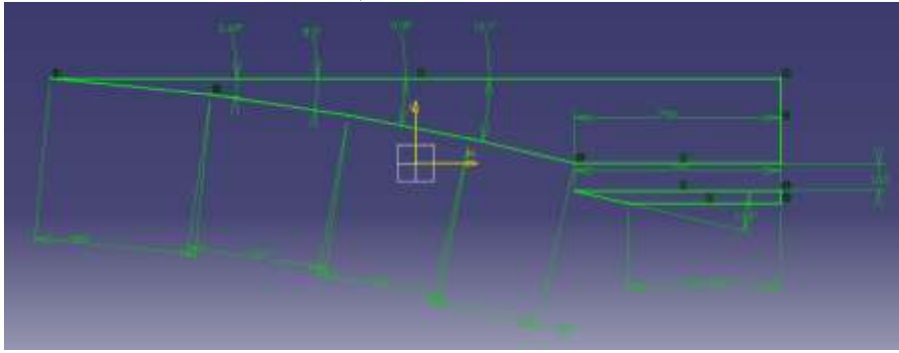


Figure1: Inlet model for Mach 8 with 4 ramps (MODEL 1)



Figure 2: Inlet model for mach 5 with 4 ramps (MODEL 2)



Figure 3: Inlet at mach 8 with 3 ramps(MODEL 3)

V. RESULTS AND ANALYSIS:

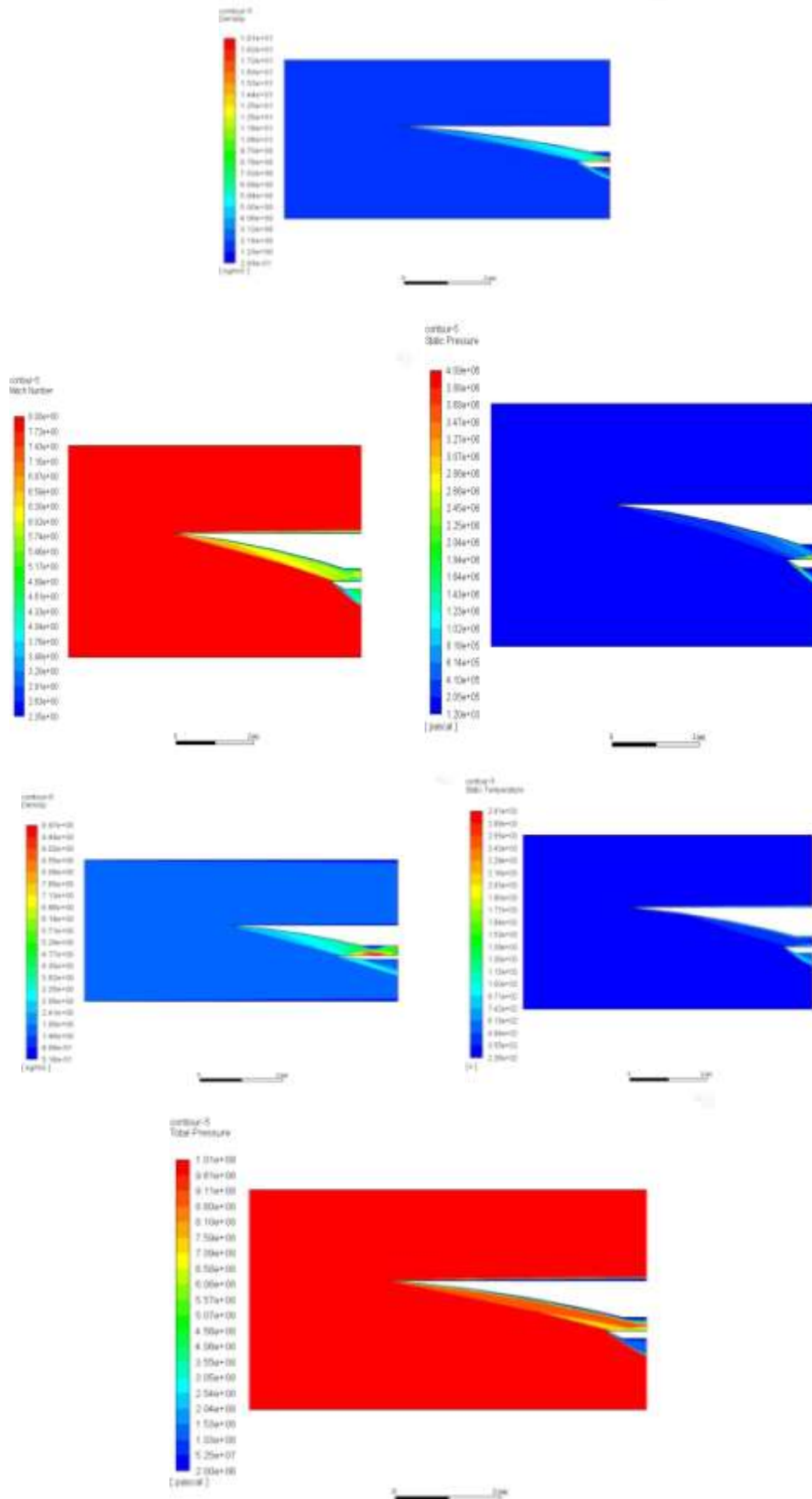
Table 1: Boundary conditions for all models

Inlet	Velocity inlet
Outlet	Pressure outlet
Upper Boundary	Wall
Lower Boundary	Wall
Fore Body	Wall
Fluid	Air
Cowl	Wall

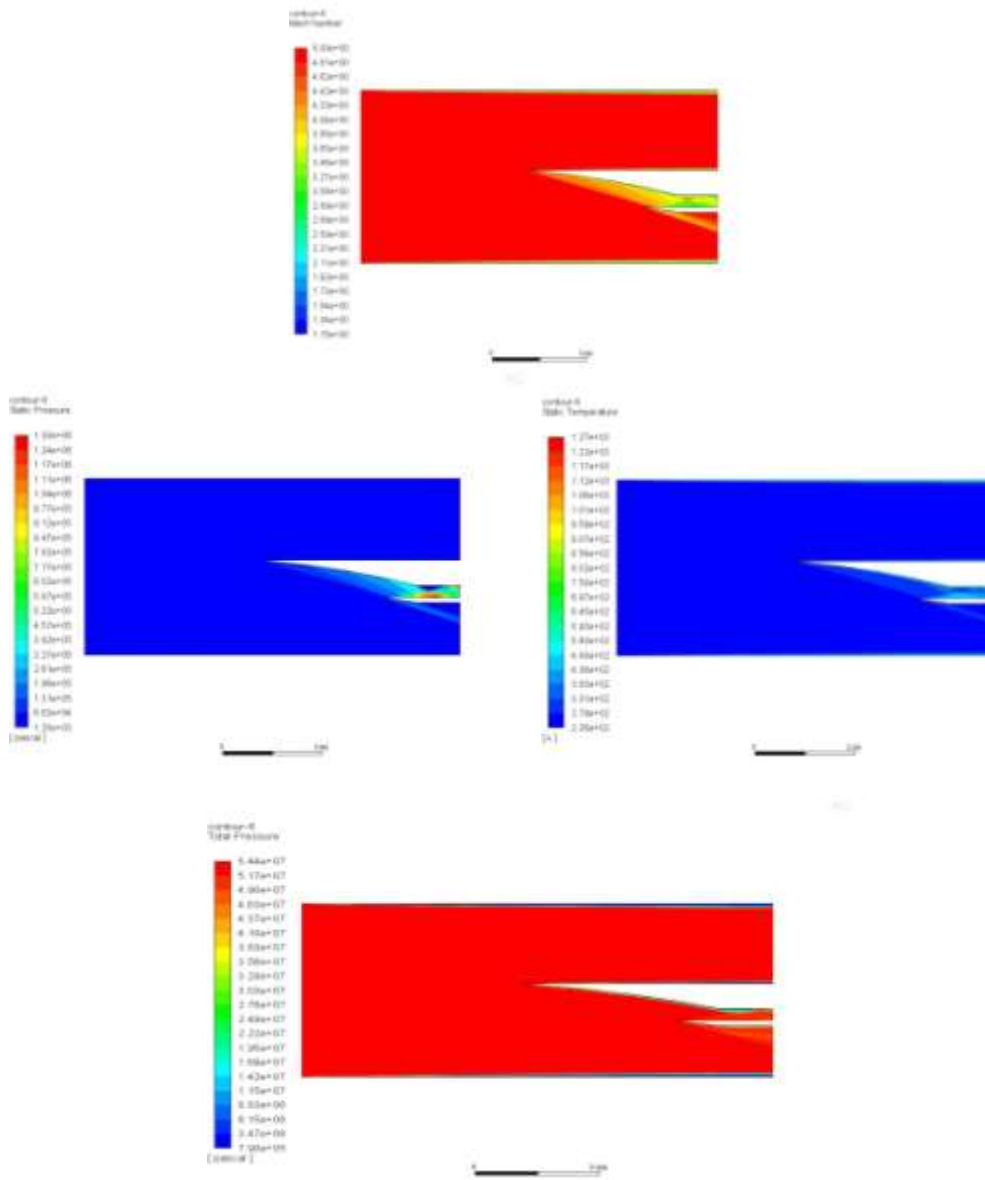
Table 2: Inlet Boundary Conditions

Pressure	1197 pa
Mach number	8 and 5
Reference Temperature	226.5 k
Turbulent Viscosity	5
Turbulent Ratio	10
Altitude	30 km

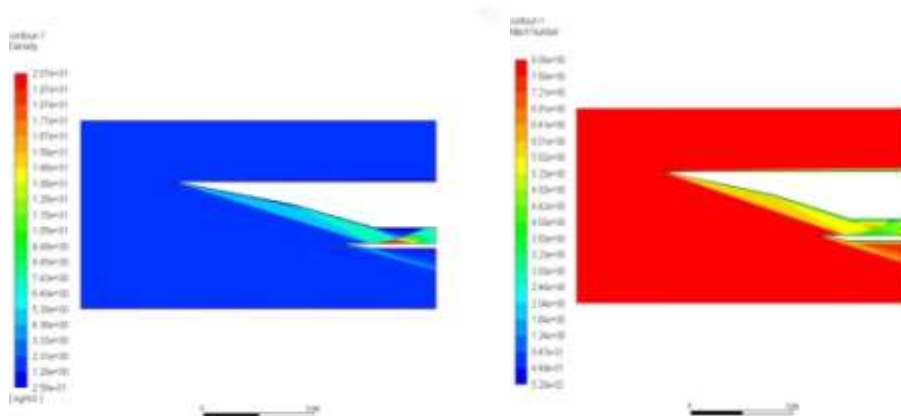
Model 1: At Mach 8 with 4 ramps.

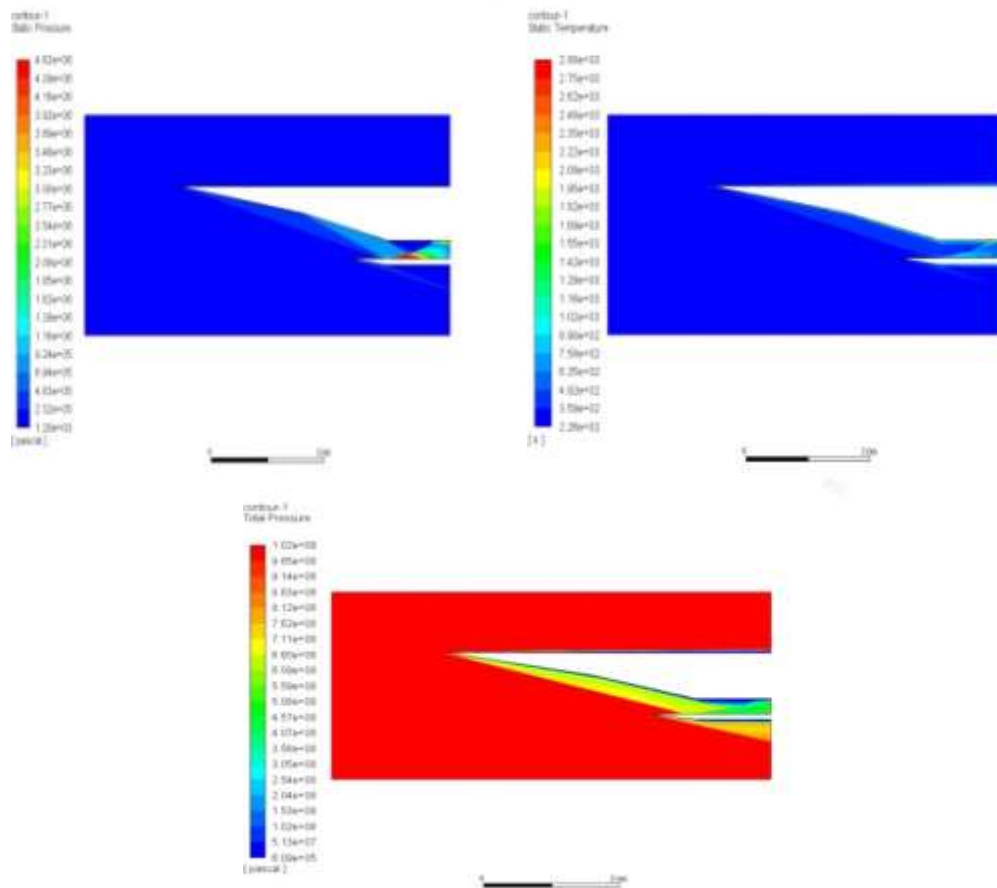


MODEL 2: AT Mach 5 with 4 ramps



MODEL 3: At Mach 8 with 3 ramps

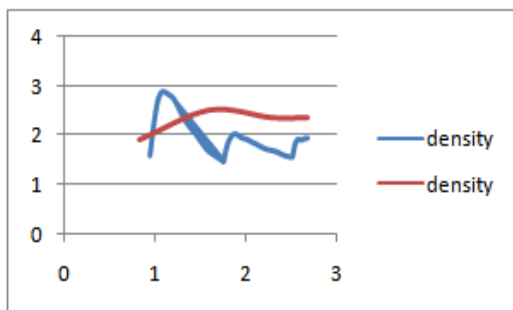




Graphical Comparison Of Theoretical And Cfd Results:

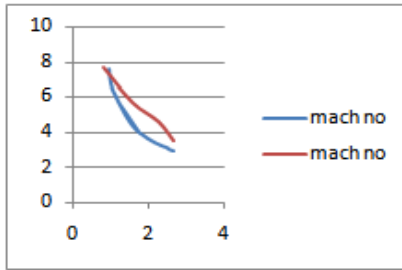
- Red line indicates theoretical results and blue line indicates CFD results.
- Length of ramp is taken on x-axis and values of static pressure, static temperature, density and total pressure is taken on y-axis.

Model 1 –At Mach 8 with 4 Ramps

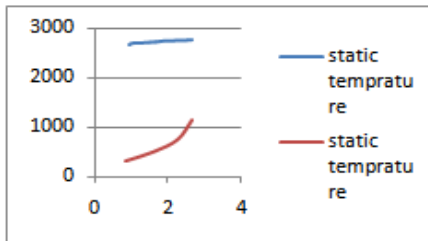


Length of ramp (m)	Theoretical value(kg/m ³)	CFD value
0.8204 (L1)	1.896	1.59959
1.5914 (L1+0.771=L2)	2.516	1.68709
2.28 (L2+0.668=L3)	2.359	1.70662
2.6788 (L3+0.398=L4)	2.359	1.95842

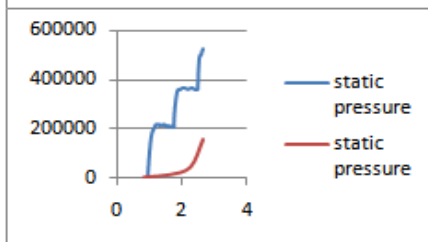
*NOTE - (0.771, 0.668 and 0.3988 are the individual ramp lengths i.e. length of ramp 2, ramp3 and ramp 4 respectively and 2.6788 is the total length of inlet)



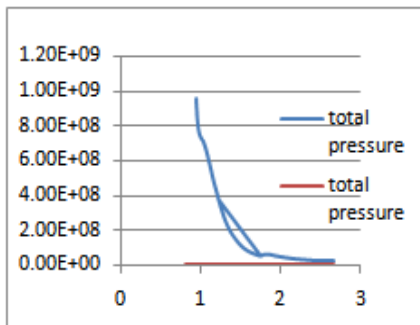
Length of ramp (m)	Theoretical value	CFD value
0.8204	7.642	7.60405
1.5914	5.697	4.3918
2.28	4.6013	3.3482
2.6788	3.505	2.96397



Length of ramp (m)	Theoretical value	CFD value
0.8204	3,027.213	5,428.27
1.5914	12,245.07	2,09324
2.28	44,241.437	3,66758
2.6788	1,59,844.40	5,27,385

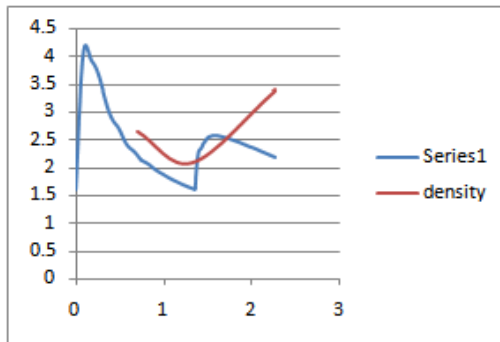


Length of ramp (m)	Theoretical value	CFD value
0.8204	302.159	2674.42
1.5914	485.85881	2719.67
2.28	744.3357	2747.74
2.6788	1,140	2762.3



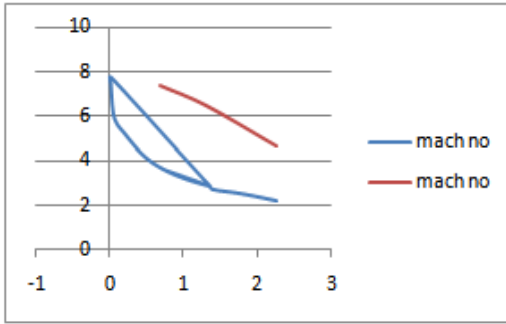
Length of ramp (m)	Theoretical value	CFD value
0.8204	7,99,168	9.60E+08
1.5914	6,13,282.124	7.86E+07
2.28	4,98,414.37	2.85E+07
2.6788	4,050,61.365	2.17E+07

Model 2 - At Mach 8 with 3 ramps

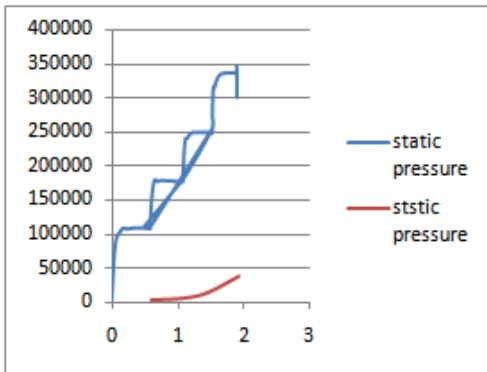


Length of ramp (m)	Theoretical value	CFD value
0.692 (L1)	2.667	2.5101
1.316 (L1+0.624=L2)	2.099	1.63695
2.261 (L2+0.944=L3)	3.4034	2.19769

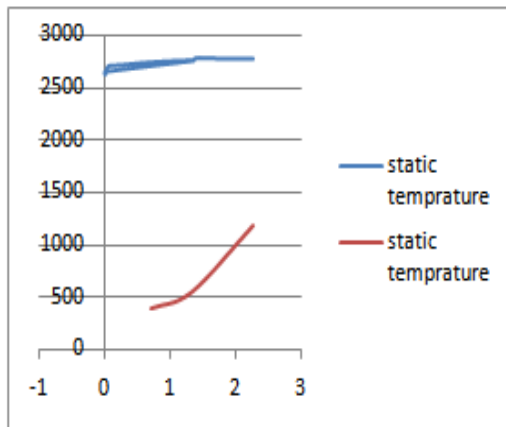
*NOTE- (0.624, 0.944 are the individual ramp lengths i.e. length of ramp2 and ramp 3 respectively and 2.261 is the total inlet length)



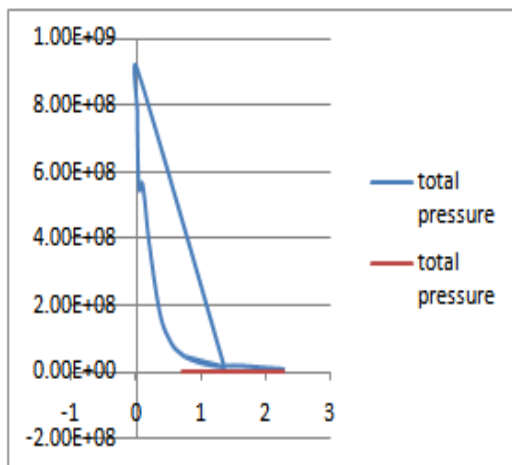
Length of ramp (m)	Theoretical value	CFD value
0.692	7.388	3.73233
1.316	6.495	2.9562
2.261	4.698	2.25793



Length of ramp (m)	Theoretical value	CFD value
0.692	5386	17,758
1.316	16003	2,492,86
2.261	1,19,691	3,469,34

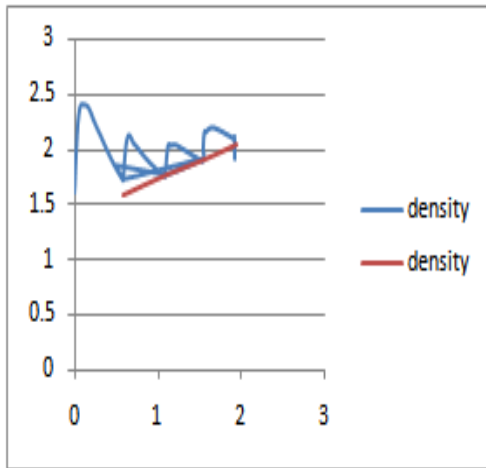


Length of ramp (m)	Theoretical value	CFD value
0.692	382.105	2741
1.316	541.06	2756
2.261	1188.71	2772



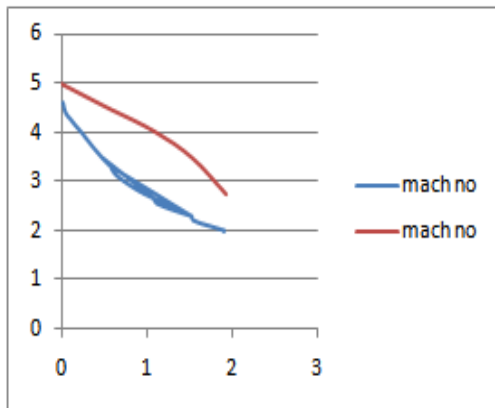
Length of ramp (m)	Theoretical value	CFD value
0.692	623980	4.29E+07
1.316	549040	1.81E+07
2.261	263154	1.10E+07

MODEL 3: At Mach 5 with 4 ramps

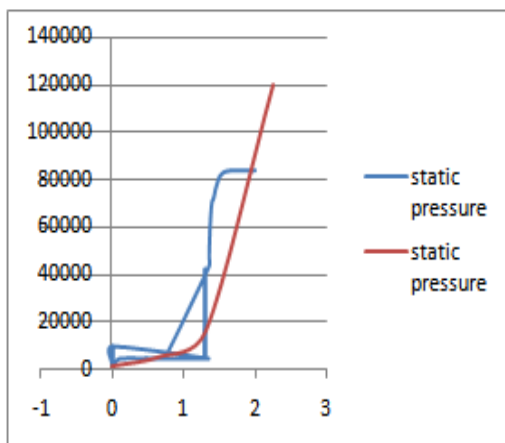


Length of ramp (m)	Theoretical value	CFD value
0.5861 (L1)	1.581	1.7277
1.0931 (L1+0.507=L2)	1.759	1.8649
1.5452 (L2+0.452=L3)	1.896	2.1059
1.938 (L3+0.392=L4)	2.032	2.1121

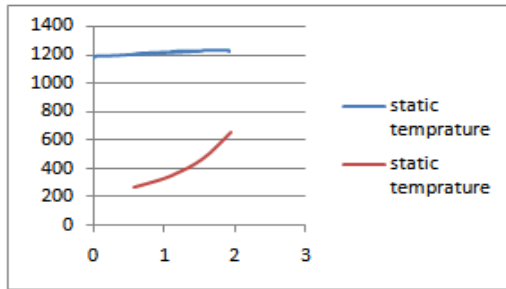
* NOTE - (0.507, 0.452, 0.392 are the individual ramp lengths i.e. length of ramp2 and ramp 3 and ramp 4 respectively and 1.938 m is the total inlet length)



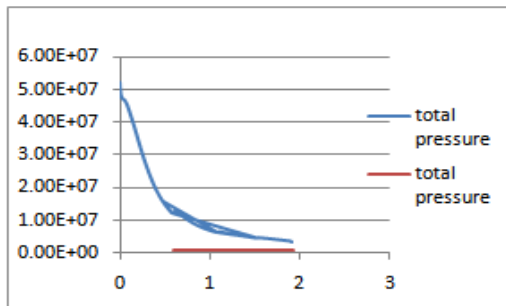
Length of ramp (m)	Theoretical value	CFD value
0.5861	4.475	3.304
1.0931	4.03	2.666
1.5452	3.478	2.278
1.938	2.741	2.021



Length of ramp (m)	Theoretical value	CFD value
0.5861	2307	4233
1.0931	5199	21,054
1.5452	13,149	31,066
1.938	37,081	84,125



Length of ramp (m)	Theoretical value	CFD value
0.5861	275.42	1203
1.0931	352.813	1219
1.5452	473.827	1228
1.938	657.673	1229



Length of ramp (m)	Theoretical value	CFD value
0.5861	841184	1.21E+07
1.0931	792,361	6.12E+06
1.5452	731,587	4.50E+06
1.938	654,917	3.10E+06

VI. CONCLUSION

Model 1

It has been observed that model one shows highest static pressure at the exit of the inlet. It uses 4 ramp configurations and is longest in length as compared to other 3 models, but as the pressure is highest can be used as scramjet is the future as scramjets can fulfill high mach number requirements at higher altitudes.

Model 2

For model 2 length was decreased in comparison to model 1, but then operating mach number was also reduced and hence its operation will be limited.

Model 3

Model 3 has is the second best model as on decreasing the ramp number from 3 to 4, there was reduction in total length when compared to model 1 and also not at much loss of static pressure at the exit of the air inlet.

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