

Performance Analysis Of Cascaded Thermal Energy Storage System Using Different Pcms

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Abstract

The sun emits energy at the rate of $3.8 \times 10^{23} kW$, out of which the earth intersects only $1.8 \times 10^{14} kW$ (Kalogeria, 2014). The remaining energy is reflected in the atmosphere. When converting intercepted energy at an efficiency of 10%, 0.1% of the energy received by the earth from the sun would be four times the world total power generating capacity. This is equivalent to the output of one hundred million modern power stations (Hankins 2012). Solar energy can be harvested for different applications that include power generation, space heating, water heating, cooking, drying etc. Though the efficiency of solar-based systems is low with a high initial cost, their usages are abruptly increasing in many sectors considering its environmental friendliness and renewable nature.

Currently, the cumulative installed capacity of solar generation across the world is 629 GW and the top installers are China, USA and India, with a generation capacity of 30,100 MW, 13,300 MW and 9,900 MW (IEA 2019), respectively. The above plants utilize photovoltaic (PV) technology for power generation, but the cost, availability and disposal of PV panel are the major raising concerns. In addition, low conversion efficiency, maintenance under extreme weather conditions, number of control components for achieving the required quality and synchronizing in a decentralized mode make their usage more complex.

Fortunately, India is blessed with abundant solar radiation, receiving 4-7 kWh of solar radiation per m^2 per day in many parts, with 300 sunny days in a year. As per the report by the Central Electricity Authority of India, the amount of solar energy received is equivalent to 5000 trillion kWh in a year, which is several fold higher than the total energy consumption of India (848 billion kWh).

The solar energy is effectively collected using a flat plate collector and a concentrating collector in a solar thermal system. The feasibility of solar thermal technologies is evaluated based on the availability of direct solar radiation and countries like the USA and Spain installed the largest capacity of solar thermal power plants. The main feature of a solar thermal system is its adaptability to energy management, ease of hybridization with a convectional system and prolong useful life. Recently, significant growth has been seen in South Africa and Morocco in solar thermal based power generation. As against the above mentioned advantages, one of the major problems is the gap between supply and demand due to the intermittent availability of solar energy. The development of suitable energy storage technology can be a promising solution for proper energy management and conservation, particularly in the medium temperature application like Solar Water Heating (SWH) system.

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INTRODUCTION

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of suitable energy storage technology can be a promising solution for proper energy management and conservation, particularly in the medium temperature application like Solar Water Heating (SWH) system. This is equivalent to the output of one hundred million modern power stations (Hankins 2012). Solar energy can be harvested for different applications that include power generation, space heating, water heating, cooking, drying etc. Though the efficiency of solar-based systems is low with a high initial cost, their usage is abruptly increasing in many sectors considering its environmental friendliness and renewable nature. In addition, low conversion efficiency, maintenance under extreme weather conditions, number of control components for achieving the required quality and synchronizing in a decentralized mode make their usage more complex.

1.1 SOLAR WATER HEATING SYSTEMS

Domestic water heating systems are known for being the second largest end-use of energy, accounting for 19% of total energy, as in general, 30 - 40 % of the electricity tariff in a family is devoted to producing hot water using electricity and natural gas (Fuentes *et al.* 2018). Thermal performance of SWH systems depends mainly on the amount of solar energy transmitted, absorbed and conducted in the collectors and also the thermal transport properties of Heat Transfer Fluid (HTF). The effective utilization of solar energy can reduce nearly 70-90% of the energy cost incurred for water heating applications. The first ever SWH system was commercialized and patented by (Kemp 1891). The SWH systems are broadly classified into the active and passive system. The first one has circulating pumps and necessary controls and not seen in the later.

1.2 Active SWH System

These systems use one or more circulating pumps for increasing the heat transfer rate and active SWH system is of two types viz. direct and indirect system. In a direct circulation system, water is circulated by the pump from storage to collectors during sunny hours. By this method, a major problem of freezing is encountered. As the circulating system enhances the energy transfer, it can be widely used in the area, where the freezing does not occur frequently. In an indirect system, working fluid is mixed with anti-freeze, circulated in a closed-loop by the pumps and the heat gained in the solar collector is transferred to water in a heat exchanger. The commonly used working fluid in these systems are the aqueous solution of glycols and the schematic arrangement of such a system is illustrated in Figure 1.2.

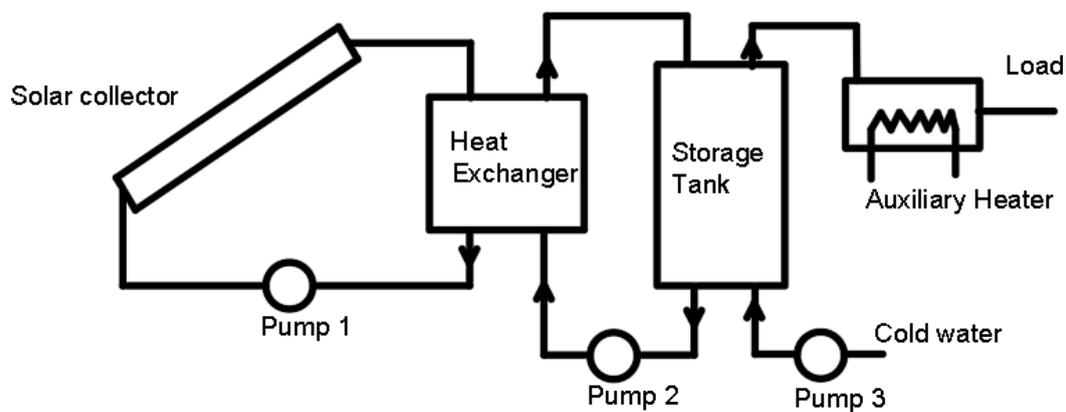


Figure 1.2 Flow diagram of an indirect SWH system

1.3 Passive SWH System

There are two types of passive systems; Integrated Collector Storage Solar Water Heaters (ICSSWH) and thermosyphon system. ICSSWH system has a storage tank, which acts as a collector as well as a storage system. This system is very useful in places, where the probability of freezing HTF is minimum. It is capable of providing hot water during an evening at the home. In the late 1900s, batch of SWH systems (ICSSWH) had been replaced by a thermosyphon system due to their pertinent heat loss problems. In this system, water flows when warm water rises as the cooler water sinks and essentially the collector must be placed below the storage tank to circulate warm water into the tank.

The main drawback associated with the system is that water with high hardness cannot be used without the presence of a water softener. The schematic arrangement of such a passive solar water heating system is shown in Figure 1.3. Though a passive SWH system is less expensive than an active system, they are not as efficient. Nevertheless,

the passive system can be more reliable and may last longer.

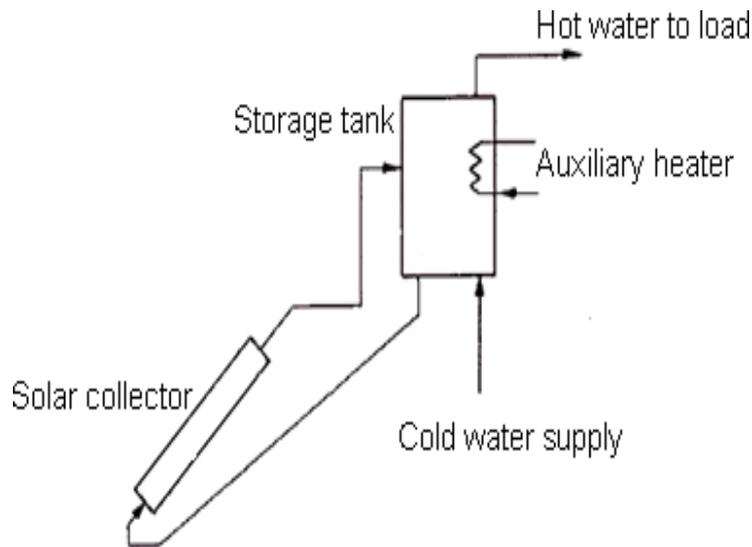


Figure 1.3 Schematic arrangement of passive solar water heating system

1.4 SOLAR COLLECTORS

Solar collectors transform solar radiation into heat and, in turn, transfer that heat to the working media like water, solar fluid or air. They are the most important critical components of any solar system. Many technical challenges need to be addressed in the effective collection of solar energy. Considerable research work has been carried out and developed new technologies on harvesting solar energy for attaining maximum collection. The solar collectors are broadly classified into

two major categories viz. tracking and non-tracking solar collectors. The first accurate model of flat plate collector was developed by Hottel-

Whillier in the 1950s and this collector was the most widely used for domestic water heating and solar space cooling/heating. A temperature up to 75 °C can be easily achieved, still the higher temperature can be obtained using heat transfer fluids other than water. Both beam and diffuse solar radiation are collected in the non-concentrated collector like flat plate collectors, and they do not require tracking of the sun and also involve low maintenance. Depending on the construction and configuration of an absorber, there are several types of non-tracking collectors as shown in Figure 1.4. A concentrating collector utilizes a parabolic shape reflecting surface and concentrates the incident solar rays to a focal line or point where the absorber is placed. These collectors only intercept beam radiation, capable of achieving very high temperature due to the concentration of diffused solar radiation in a smaller area (Kumaresan *et al.* 2017).

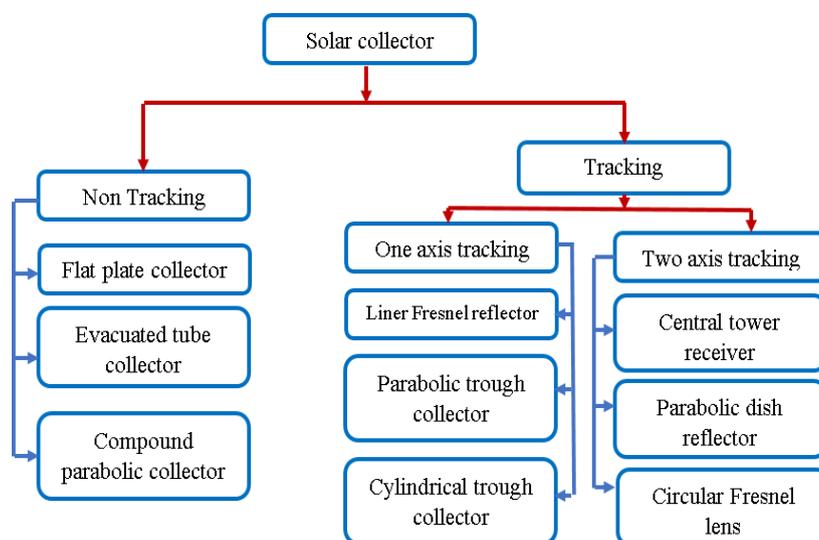


Figure 1.4 Classification of solar collectors

Despite the advantages of concentrating collectors like higher thermal efficiency, the requirement of less material and low cost per unit area over the conventional flat plate collector, there are certain disadvantages as given below:

- Depending on the concentration ratio, only little diffuse solar radiation can be collected.
- The concentrating collectors cannot follow the daily motions of the sun due to its apparent movement across the sky. This necessitates the requirement of complex tracking mechanisms, that involve more expensive components.

Increasing attention has been seen on the development of stationary solar collectors with a Compound Parabolic Concentrator (CPC). This type of collector operates over a wide range of operating temperature, capable of collecting both direct beam radiation and part of diffuser radiation. The collected radiation is concentrated on the stationary absorber tubes (Orosz & Dicks 2017). By using multiple internal reflections, any radiation entering the aperture area of the collector is focused to the absorber surface by CPC, placed at the bottom of the collector. The CPCs are designed either symmetric and asymmetric and the main features of CPC are described in the following section.

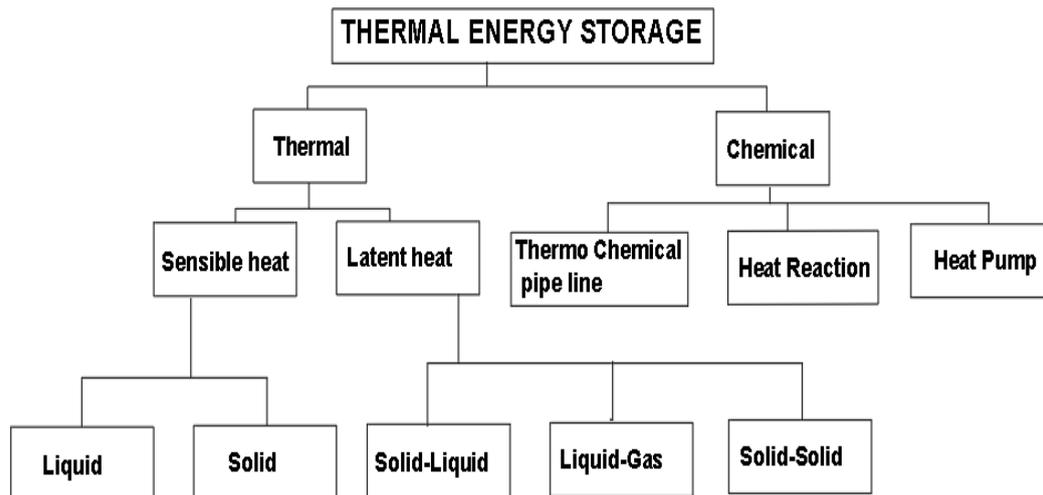
1.5 Compound Parabolic Collectors (CPCs)

Pioneering work was carried out on the concept of the three tracking concentrating static concentrator by Tabor in late 1950s. Studies by Hinterberger & Winston (1966) explored the importance of non-imaging concentrators in solar thermal applications. CPC can accept incoming radiation with a wider range of angle, focusing on the absorber through multiple internal reflections. A gap is maintained between the receiver and reflector in the CPC to prevent losses. The gap should be small and an increase in gap leads to a loss of thermal performance due to a reduction in the reflected area. As there is no need for tracking collection of part of diffused radiation, the CPC solar collector is more effective than Parabolic Trough Collector (PTC) in attaining HTF temperature nearly up to 300 ° C (Karwa *et al.* 2015). Moreover, its capability of collecting diffuse radiation during cloudy days is advantageous in areas where the percentage of diffused radiation is high (Widyolaret *al.* 2018). Growing interest recently seen in domestic and industrial sector makes the CPC technologies more relevant for low and medium temperature applications. The tubular absorber CPC is more suitable for the SWH system, yielding relative higher heat collection efficiency.

2.1 THERMAL ENERGY STORAGE SYSTEM

Thermal Energy Storage (TES) system is a technology that helps storage of thermal energy by heating or cooling in a storage medium so that the stored energy can be utilized at a later time. TES system is widely used in application like buildings and different industrial process, where nearly half of the energy consumption is in the form of thermal energy. Variations in energy demand in these sectors are seen during the day and between the days. TES system can reduce the mismatch between energy supply and demand. Moreover, deployment of TES system reduces decarbonization of the electric grid, heat demand and cost. The global market size of TES is projected to USD 8 billion for the year 2027, owing to the continuous shifting towards renewable energy sources which are highly intermittent in nature (Global Industry 2020). The benefits of TES integration with renewable energy sources include an increase in the share of renewables in energy needs, becoming particularly important in the solar water heating application, when the sunlight is not available.

TES system is the most promising one, as the stored energy can be directly consumed in the form of hot or cold energy, minimizing the energy losses during conversion in different applications (Alptekin & Ezan 2020). Energy can be stored either in the form of sensible or latent heat; the LHTE system possesses a higher energy storage density, capable of storing or retrieving energy in a nearby isothermal condition (Suresh & Saini 2020). In the former case, a sensible heat storage system is relatively less expensive. However, its low energy density about 3-5 times lower than that of a latent heat storage system requires a larger volume. In addition to the above two types of TES system, a thermochemical storage system is also being used for different applications in which energy is stored and released by the breaking molecule bond in the chemical reaction. The major classification of a thermal storage system is presented in Figure 1.10.



(Source: Sharma *et al.*, 2009)
Figure 2.1 Classification of TES systems

2.2 Latent Heat Storage System

Latent Heat Thermal Energy Storage (LHTES) system works based on the principle of storing or releasing heat when a storage material undergoes a phase change transition from solid to liquid or liquid-solid, which may also be accompanied by the sensible heat. The potential utility of a thermal storage system using materials undergoing solid-gas and gas-liquid is ruled out. Although using solid-solid phase change is free from the containment design problem, the low latent heat of these materials makes them not suitable for TES application. Solid-liquid phase transition is more attractive due to negligible volume change.

Nowadays PCMs can be used in LHTES applications, storing the heat during solid-liquid phase change processes or vice versa and providing a large heat capacity over a limited temperature range. When the temperature of PCMs reaches the melting temperature, PCMs change the phase from solid-liquid, absorbing the heat as the reaction is endothermic. Similarly, when the temperature of PCMs reaches the below solidifying temperature, PCMs change their state from liquid to solid, releasing the stored energy.

The amount of energy stored per unit mass during the melting period is determined from Equation. where, m - mass of PCM (kg), c - specific heat ($J kg^{-1} K^{-1}$), a_m - fraction melted

2.3 Phase Change Materials

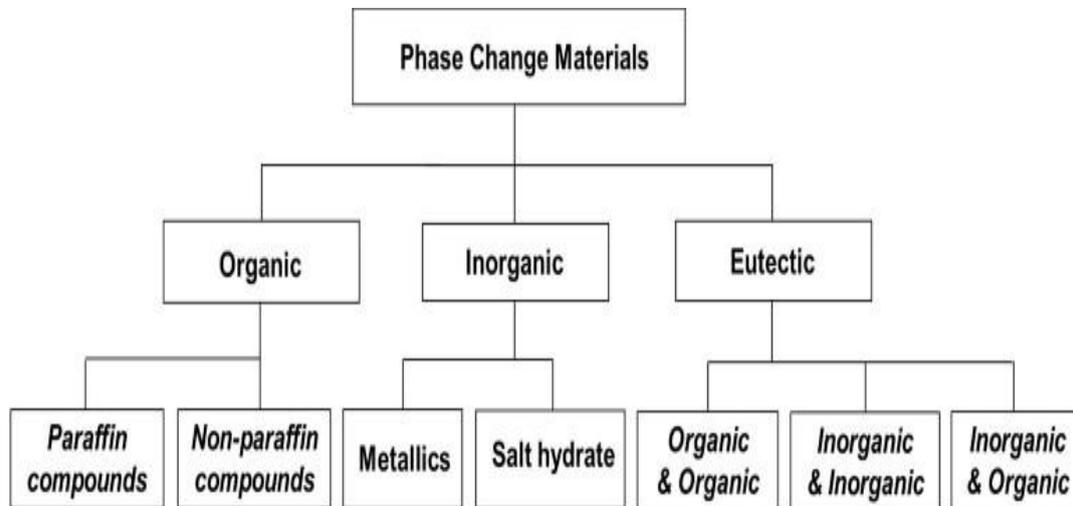
Phase Change Materials (PCMs) are substances that possess large latent heat and a range of phase transition temperature. It is important to highlight a crucial feature of the matching of phase transition temperature range to take advantage of the latent heat involved in the solid-liquid phase change process. The PCMs are mainly grouped into organic, inorganic, eutectic mixtures as shown in Figure 1.11. Among these, paraffin received greater attention due to higher storage density, congruent melting/solidification occurring without any subcooling, non-reactive to other chemical reagents, and they are water repellent (Kumaresan *et al.*, 2012). A wide variety of non-paraffin PCMs such as fatty acid, ester, alcohol and glycols are available and their application in TES has been reported by (Sharma *et al.*, 2009). The major advantages and disadvantages of each category of PCMs are summarized in Table A1.2 as given in Appendix I. Numerous PCMs are commercially available in the phase transition temperature ranging between 30 °C to 600 °C and some of the commonly used PCMs in a solar thermal application is listed in Table A1.3 as given in Annexure I. They can be used for several cycles of heating/cooling mode without thermal degradation. PCMs with high latent heat can offer a nearly isothermal heat exchange with a higher storage per unit volume. Despite various relative merits mentioned above, the thermal performance of PCMs is hindered through incomplete melting and solidification. This leads to a lower energy storage density mainly due to its poor thermal conductivity (Zhao *et al.*, 2018). Practically, the above-mentioned drawbacks are different from each other that need to be addressed for enhancing the overall performance.

Various methods have been proposed in the past for enhancing the thermal performance of LHTES system that include the dispersion of high thermal conductivity particles in the PCMs (Pramothraj *et al.*, 2019; Chandrasekaran *et al.*, 2014; Kumaresan *et al.*, 2012)

),employingextendedsurface (Elfekyet *al.* 2018; Seeniraj& Narasimhan 2008), metal foam/metalmatrix, implementing the cascaded arrangement of PCMs (Farid &Kanzawa1989; Farid *et al.* 1990), dispersion of PCMs into geometric stability structure(Ehid& Fleischer 2012),and the addition of nucleating reagent into PCM(Vikrametal.2019).Eachoftheabove-mentionedtechniquehasbeenstudied in recent years. But, there is no single technique found as superior forperformance augmentation of the LHTES system. The choice of a specific technique is left to the designer's concern on a case to case basis depending onthe scope of an application. Addition of extended surface and dispersion ofhigh conductive particles for a given system could contribute to enhancedenergystorage rate(powerdensity).However,employingcascadedPCMsand micro-encapsulation of PCMs enhance both energy storage and powerdensity(Narasimhan2019).

The following thermal physical properties of PCMs should be takeninto consideration in the designing of any LHTES system for any specificapplications.

- Thedesiredphasetransitiontemperature.
- Latentheat offusionperunitmassshouldbe high.
- Highthermalconductivityshouldbehighduringliquidandsolidphases.
- Theminimumchangeinvolumeanddensityduringthephasetransitiontime.
- Minimalsub-coolingatthetimeof freezing.



(Source: Sharma*etal.*2009)
Figure2.3ClassificationofPCMs

Inaddition,tothat,thePCMs shouldnothaveasignificantenvironmental impact during their life cycle. It should be remarked that thebehaviourofcommercialPCMsisdifferentfromtheidealPCMs.Theenthalpy curves of commercial PCMs are different from theidealone owingto the existence of subcooling and difference in thermal cycle stability. These curves could be impacted by a commonphenomenonlikesubcooling, andcycle stability. The major problems in PCMs based TES system are phaseseparation and segregation. A reduction in phase change enthalpy of PCMs exhibits phaseseparation after repeated cycling. Considerableresearchworkis being carried out in thefieldof PCMsbased TES system and thehotstorage systems have been deployed in industrial applications. The comparison study between sensible heat and latent heat storage material for the stored energy of 4.18×10^6 kJ in terms of mass and volume of the material can be seen from Appendix 1 (Table 1.4).

The implementation of the TES system with solar collector has the following advantages:

- The provision of a TES system can make a significant reduction in the consumption of auxiliary energy in most solar systems and dramatically increase the so-called solar fraction.
- Variations in solar irradiance can cause an instantaneous change in energy generation (i.e., power or heat). These strong variations impact not only the availability of energy, but also the consistency of the power grid. Coupling of the TES system into the solar system can enhance the thermal inertia, reduce the fluctuations and system stability.
- Energy demand during peak hours cannot accord with the peak solar radiation. TES system can enhance the dispatchability of a solar system by storing heat energy at the time of off-peak hours and retrieve it at the time of peak hours demand. This results in matching the energy generation and demand and also enhances profitability as the peak-hour electricity tariffs are higher.

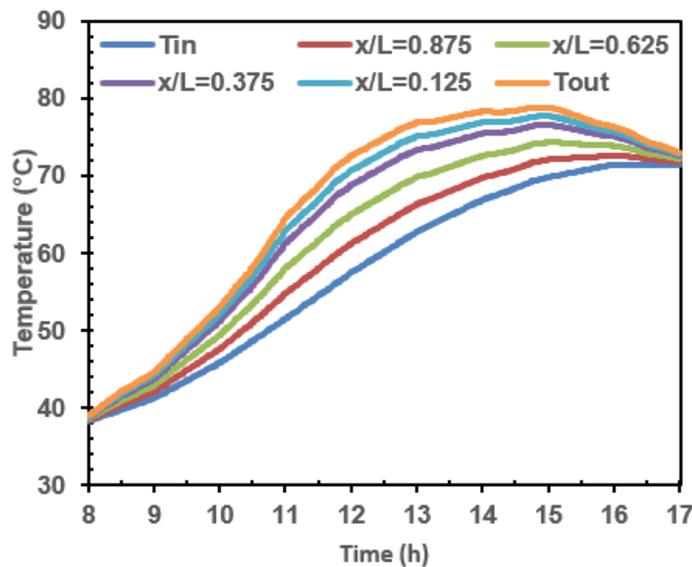
- Reduction in overall heat loss coefficient, resulting in enhancement of thermal efficiency and downsizing the SWH system.

Results and discussion

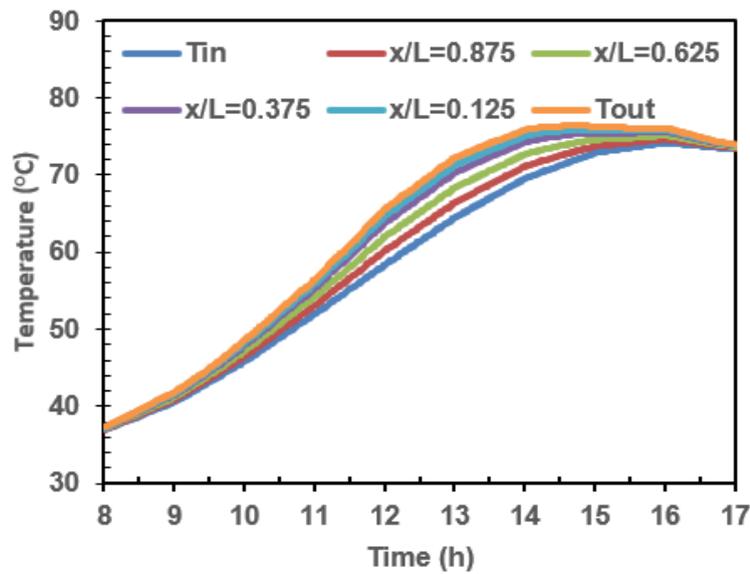
3.1 Selection of PCMs

It is necessary to determine the degree of stratification along the flow direction of the HTF using a sensible heat storage medium to select the appropriate PCMs. The experiments were performed at different flow rates of 60 kg/h, 120 kg/h and 180 kg/h. Time-temperature (T-t) history of HTF at different locations inside the TES tank is presented in Fig 3 (a-c). As seen from the figure that the initial temperature of the HTF in the storage tank varies from 35-36 °C for all three different flow rates. The average rise in the temperature of the HTF in the TES tank is insignificant from 8.00 h-9.00 h, even though the temperature across collector is higher as shown in Fig 3 (a). The reason is that the high thermal inertia associated with the experimental components. After that, the HTF temperature in the storage tank progressively increased until 13.00 h and further increased is seen till 15.00 h. After 15.00, average HTF temperature in the storage started to decline. The reason is energy collected by the solar collector is less compared losses taking place during the HTF flow through pipes and storage unit. The similar trend is observed in the HTF plot for the other two flow rates as depicted in Fig 3 (a-b). Hence from the graphs, it is observed that temperature profile of the HTF varies on two input parameters such as solar radiation and mass flow rate. Based on the experiments conducted on three different day with three different flow rates the maximum and minimum temperature of HTF at each zone are arrived.

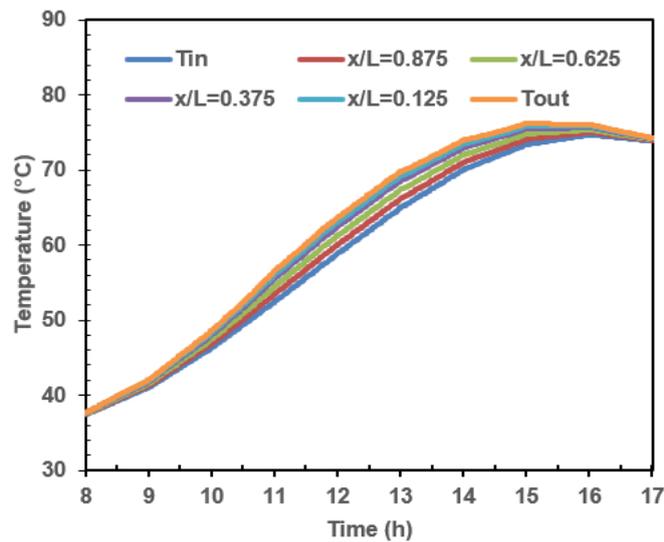
The minimum temperature of HTF is taken as a reference temperature for the given zone to select the suitable PCMs to be placed in a particular zone. In order to achieve the complete charging process, the PCMs melting temperature in each zone is selected based on the minimum HTF temperature with driving potential of 7 °C for top zone ($x/L=0.125$), followed by 14 °C for next-two zone ($x/L=0.375$ and $x/L=0.625$), and 21 °C bottom zone ($x/L=0.875$), respectively. The reason for selecting PCMs linearly along the storage tank height is that once the top zone is filled with PCM, the part of the HTF temperature profile reduces their slope [21]. Further, it is also understood from the above experiments that the stratification effect predicts the range of PCMs can be placed in a particular location, whereas it cannot identify the right temperature meting point for the given condition. In the present studies, the experiments are conducted by placing six different PCMs as shown in Fig 2 and in which the selection of PCMs was done based on the degree of stratification temperature. The thermophysical properties of the selected PCMs for the present work is given in Table 4.



(a)



(b)



(c)

Fig.3.1 Temperature plot variation of HTF at different flowrate (a) 60 kg/h, (b)120 kg/h, (c)180 kg/h

3.2 MIX number

A simple way of showing the degree of stratification of a TES is by 2D plots. As the temperature profile does not give the information in the best way to characterize the stratification in a water storage tank, dimensionless numbers called MIX numbers is used which condense this information in a single parameter. Fig.8 shows the MIX number of HTF at a flow rate of 60 kg/h, 120 kg/h and 180 kg/h. A non-dimensional time, which is instantaneous time by the total charging time, was utilized to depict the MIX number. The various mass flow rate shows very comparable MIX number plots during the charging process. At the start of charging process, the MIX number goes from higher value to lower value for a particular time period, followed by lower MIX number to higher MIX number, this indicates stratification and destratification effect in the storage tank. This is because the overall temperature gradient in the storage tank increases during the charging process for a certain period and after that overall temperature gradient started to degrade in a storage tank. Similar trend of the MIX number are seen with the mass flow rate of 120 kg/h and 180 kg/h in Fig.8. For the low mass flow rate of 60 kg/h, the MIX number was minimum as compared to the other flow rate, announcing that mass flow rate of 60 kg/h could maintain larger stratification effect for maximum duration compared to other two cases. Moreover, the MIX number during peak value for 60 kg/h, 120 kg/h and 180 kg/h are 0, 0.44 and 0.59. The result implies that, once the flow rate increases from 60 to 120 kg/h and 120 to 180 kg/h the stratification effect was reduced to 56 % and 34 % respectively. Thus, it is construed that storage tank attains better stratification for varying heat load at a lower flow rate compared to a higher flow rate.

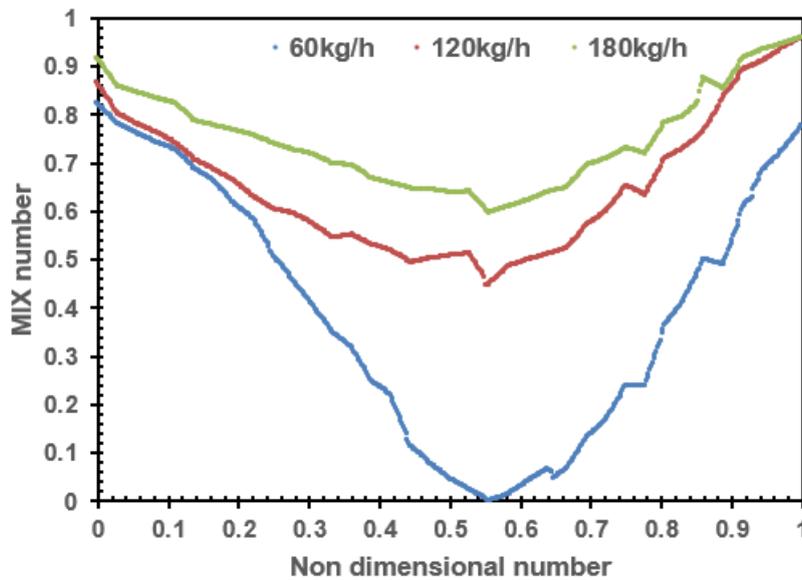


Fig.3.2 MIX number for various flowrates at varying heat load.

3.3 CUMULATIVE ENERGY

The cumulative energy retrieved by HTF during discharging process. It is seen that time require for retrieving 18817 kJ, 21008 kJ and 23564 kJ are 125 min, 96 min and 57 min for the mass flow rates 60 kg/h, 90 kg/h and 120 kg/h respectively. From the temperature point of view (Fig 12), it is observed that the higher the mass flow rate were, the faster PCMs is discharged. The temperature difference between the PCMs and HTF stay higher as the flow rate increases and also the losses associated with the outlet heat transfer rate also reduced considerably for higher mass flow rates. Due to this at higher flow rate the energy retrieving capacity of HTF for given stored energy is higher compared to other two flow rates.

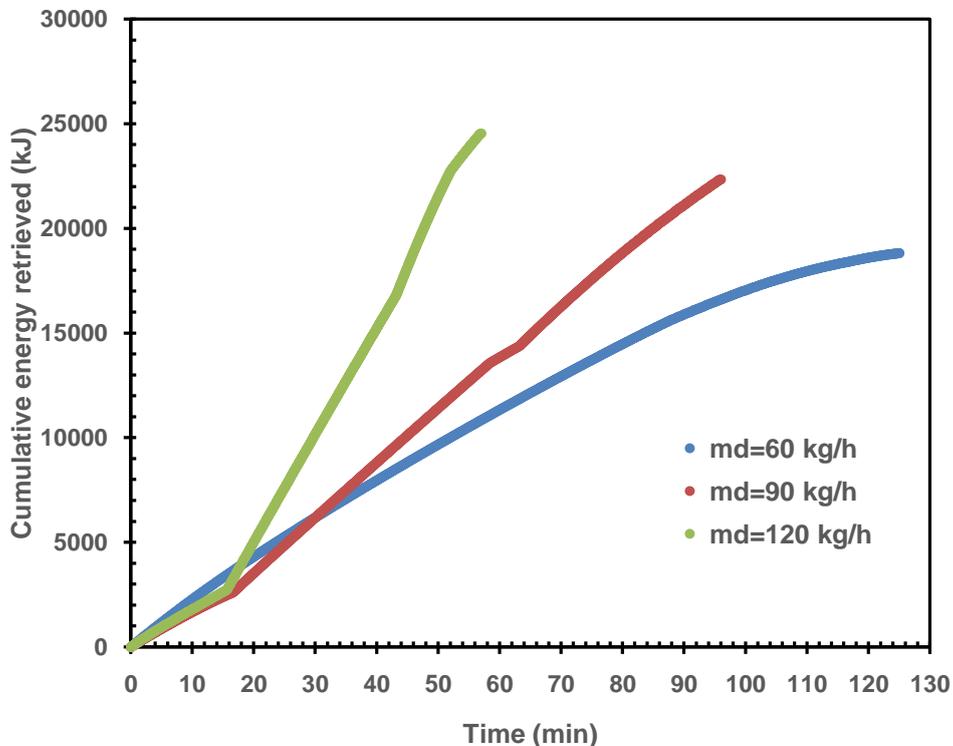
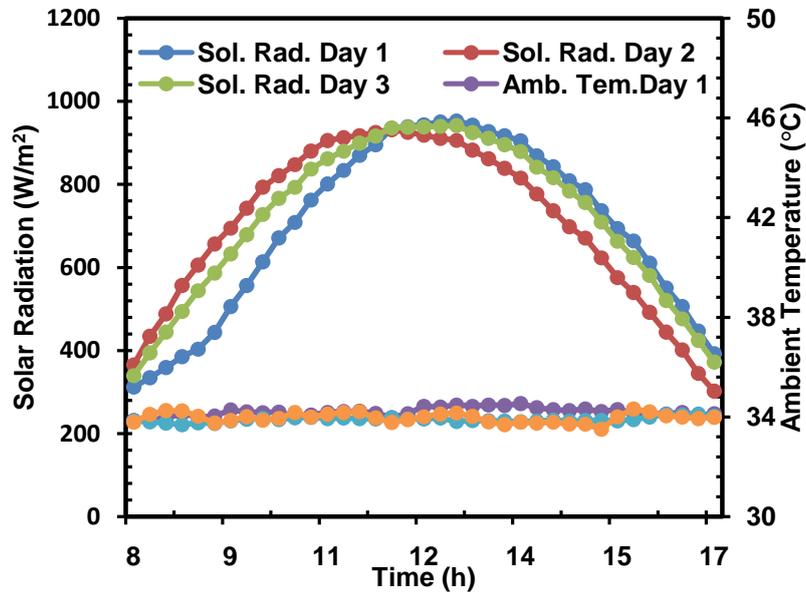


Fig.3.3 Cumulative energy retrieved by the HTF from the cascaded LHTES system

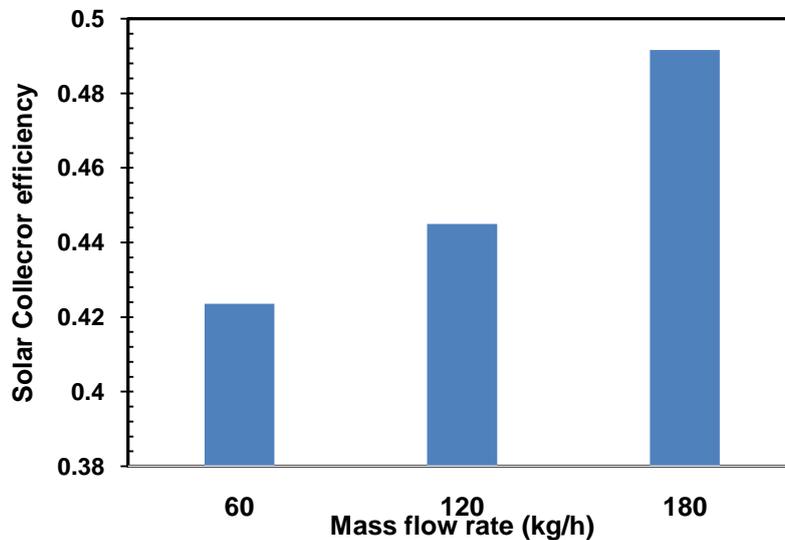
3.4 Efficiency of CPC solar collector

The solar radiation, mass flow rate and temperature difference between inlet and outlet is considered as an important key factor while calculating the system efficiency. Thus, the variations of collector efficiency

along with ambient temperature and daylight hours for various mass flow rate are depicted in Fig. 12 and 13. It is observed from the plot that these three days of the solar irradiation and ambient temperature don't have sensible change to affect the final comparison results. As the flow rate increases the heat transfer coefficient between the HTF and solar collector absorber plate was increased. Due to the increase in heat transfer coefficient between absorber tube and HTF, the overall heat loss coefficient in the solar collector got reduced considerable. As a result, the energy gain by the HTF fluid got increased, due to which the thermal efficiency of solar collector increased by increase in flow rate with the percentage 42 %, 44 % and 49 % respectively.



Hourly variation of solar radiation and ambient temperature



Effect of solar collector efficiency for various flow rates

Conclusions

An experimental study of the performance evaluation of a CPC collector, integrated with a cascaded LHTES system is carried out. The performance study of the CPC collector and the cascaded LHTES system has been conducted during full sunny days. The temperature evolution of PCMs and HTF during charging and discharging processes are studied. The collector efficiency, energy stored and retrieved in the cascaded LHTES system and thermal stratification behavior are estimated and the major conclusion is drawn as given below:

- During charging process, it is noticed that the latent heat of the PCMs are completely utilized for the given time. These observations show that the PCMs arrangements made within the storage tank are in the right configuration for the given experimental condition.

- The simultaneous phase transition were seen for six PCMs in three different flow rates. It is due to the minimum temperature band gap between PCMs, surface convection and nearly uniform temperature driving potential between the PCMs and HTF throughout the storage tank.
 - The cumulative energy stored at any instant of time increases with increase in flow rates for given inlet HTF temperature. It is due to higher energy content associated with the HTF for higher flow rates. The stratification behavior was studied using MIX number and the result revealed that stratification effect was influenced by the HTF flow rate, the incoming solar radiation to the aperture area and out let of HTF temperature from the solar collector.
 - The solar collector started to increase their efficiency as the flow rate progress. The improvement is due to enhancement in the internal convective heat transfer rate as the HTF flow increases. The thermal efficiency of solar collector increases from 42 % to 49 % as the flow rate increases from 60 kg/h to 180 kg/h.
 - In the present work discharging was conducted during night time after completion of charging process. It is inferred that the HTF attain a nearly an isothermal temperature once the latent of different PCMs in the storage tanks was capture simultaneously.
- The above PCMs configuration integrated with solar collector is best suited to meet the domestic hot water demand for Indian climatic conditions.