

Effectiveness of Condition Monitoring on Screw Compressors

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ABSTRACT:*Purpose –In recent years, screw compressors have seen a large increase in popularity particularly in compressed air and refrigeration service. Screw compressors are positive displacement compressors that utilize a pair of helical lobed rotors in a casing. The screw compressor has no valves;therefore, the location of the suction and discharge ports determines the compressor cycle. This study focuses on the condition monitoring of a screw compressor in instrument air service. Condition monitoring through vibration analysis and oil analysis are heavily relied upon in industry to determine maintenance requirements. This paper examines each technology’s ability to provide advanced notification of mechanical faults in screw compressors.*

Design/methodology/approach – The research analyzes the ability of vibration analysis and oil analysis on a screw compressor in an oil and gas plant. The vibration data and oil data were collected from commissioning thru failure. The data is presented to demonstrate each technology’s ability to provide advance warning of the failure.

Findings –The study considers utilizing condition monitoring technology to provide early screw compressor malfunction warnings. The results of the study indicate that both vibration analysis and oil analysis provide early warning of pending mechanical failures. Oil analysis was found to be more effectiveat providing advance notice.

Originality / value –The study reveals the advanced malfunction warning capabilities of implementing condition monitoring technologies in the form of vibration analysis and oil analysis on screw compressors.

Keywords – *Condition monitoring, vibration analysis, oil analysis, screw compressor, particle count, contamination code, overall vibration*

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I. INTRODUCTION

An estimated 17% of the world’s electrical power generated is consumed by compressors used in a combination of industrial, commercial, and domestic applications. The current world compressor production rate is in excess of 200 million units per year with the majority of these being the positive displacement type. Compressed air and refrigeration systems account for most of the manufactured units (Stosic, 2004). In a study conducted by Eti et al. (2006), it was reported that even the world’s best performing organizations within the petrochemical industry still incur annual maintenance costs of up to 2% of the present replacement values of their plant assets. As screw compressors continue to gain acceptance, they will be utilized in more critical processes throughout production facilities. The increased reliance on screw compressors will require a high level of reliability to meet production demands.

Maintenance strategies that are commonly used in industry can be classified into the following three categories: corrective maintenance, preventive maintenance and condition based maintenance (CBM) (Bevilacqua and Braglia, 2000). Corrective maintenance takes action only when an asset breaks down. Preventive maintenance performs inspections, replacement and overhauls on a schedule based on historical failure rates. CBM schedules maintenance work based on the results from condition monitoring technologies. It is crucial to determine the optimal condition monitoring techniques to utilize in order to effectively schedule maintenance activities. CBM of compressors relies heavily on vibration analysis and oil analysis technologies to be implemented effectively. Vibration analysis is a tested and proven technology that continuously improves due to processing speed improvements, which in turn, speed up the data collection process. Oil analysis is a well-established technology that is often reserved for large turbomachinery generally requiring outsourcing to a third party laboratory for analysis.

Condition Monitoring

CBM is a maintenance strategy that continuously surveys the working conditions of the machine to determine the timing and type of required maintenance (Veldman et al., 2011). CBM uses condition monitoring information obtained from data acquisition systems to enable diagnoses of imminent faults and diagnoses regarding the machines remaining useful life. If the anomaly is catastrophic, operators can shut down the

machine immediately. Otherwise, operators can decide to continue operating the machinery under faulty conditions until the end of the predicted remaining useful life (Ruiz-Carcel et al., 2016). Therefore, CBM allows maintenance work to be scheduled on an as needed basis, an attractive alternative to traditional strategies.

Condition monitoring assesses the compressor's health by analyzing parameters such as vibration, flow rate, indicated horsepower, motor amperage, temperatures, pressures, lubrication and wear debris analysis (Townsend and Badar, 2018). Despite the significance of the achievements recorded using each of these condition monitoring techniques, vibration analysis of rotating machines is the most prevalent in terms of applicability and popularity. This is due to its ability to provide a reasonable lead time to the failure for most rotating machines (Yunusa-Kaltungo and Sinha, 2014; Yunusa-Kaltungo et al., 2014). Condition monitoring has evolved over time with practitioner experience. For instance, Galar et al. (2010) realized that the existing rules for rotating machine maintenance intervals provided by original equipment manufacturers are often static and do not necessarily reflect age and operational context of the machine which sometimes trigger unnecessary maintenance interventions.

Rotating equipment is made up of countless parts in which relative motion is transferred from one moving part to another generating significant sound and vibration. According to the principles of mechanisms, each moving part in the machine has an individual vibration signal. The signal changes along with the change in the state of machine parts, the change in the vibration signal is an indication of fault in the machine's incipient stage that can be detected and repaired before failure. The main application of condition monitoring is data collection and evaluation to identify changes in performance. The main advantage of condition monitoring is to detect the condition of machine components by utilizing selected measurements to identify the changes in operating condition as depicted below (Kiran Kumar et al., 2018).

- Condition monitoring gives warnings before final failure.
- Condition monitoring gives the nature of failure and information.
- Condition monitoring manages the machine life potential.
- Condition monitoring evaluates corrective action.
- Condition monitoring improves maintenance efficiency and reduces risk and saving money.

CBM is advantageous to plants as machine faults can be detected before failure occurs, without doing regular scheduled maintenance. This maintenance philosophy requires regular and frequent monitoring of the machine operating condition. Practices such as vibration analysis, infrared thermography, ultrasound and various other forms of non-destructive testing can be used to detect deterioration of machine operating condition and problems in the components before they fail and require a plant shut down. Usually critical plant equipment undergo this form of philosophy because it helps in reducing downtime, detecting root cause of the failure and managing resources such as labor and spare parts effectively. A proactive maintenance philosophy is the best way to manage and maintain the components and equipment in a plant, but only if used effectively and in required places, otherwise it can get very expensive. It is important to find defects with the equipment before failure to avoid affecting the condition of equipment components and further damage to the plant (Senapaty and Rao, 2018).

Screw Compressors

The release of API Standard 619 1st Edition – Rotary Type Positive Displacement Compressors for General Refinery Services in 1975 led to the widespread recognition of screw compressors. According to the standard, "Screw compressors find use in many chemical services. Most significantly, they are employed where no other compressor will work or is economic. They tolerate more abuse than any other comparable unit. On low molecular weight, they enjoy the same benefit as reciprocating compressors since the significance of flow density is not detrimental as in the case with centrifugal compressors" (API, 1975). Due to increased usage in recent years, screw compressors have effectively displaced reciprocating compressors in the medium displacements and are now the most popular compressor type in their size range. With the inception of larger displacement screws, they are intruding further on the lower end of the centrifugal sizes (Pillis, 1999).

A screw compressor is composed of male and female rotors mounted in bearings to maintain their location in a rotor housing that holds the rotors in close tolerance intersecting cylindrical bores. See figure 1 for typical screw compressor rotors. Rotors are currently made using grinding machine tools with simultaneous measurement, control, and correction of the profile, which makes it possible to achieve a dimensional tolerance of 5 μm , which enables the clearances between the rotors to be maintained below 15 μm . With such close clearances, there is a potential for rotor contact and therefore the profile and its clearance distribution must be created in a manner that damage or seizure will be avoided should contact take place (Stosic, 2004). The bearings provide proper positioning and rotating ease while transferring a load between shaft and housing (Kaldarno et al., 2008). The fundamental shape of a rotor is a screw thread, with differing numbers of lobes on the male and female rotors. Screw compressors have become known for reliability, flexibility, low maintenance, and good

efficiency in multiple industries. However, the main reasons for unscheduled shutdowns of screw compressors are bearing issues and seal problems (Davidson & Bertele, 2000).

Screw compressors are positive displacement equipment that utilize a pair of intermeshing rotors as opposed to a piston to produce compression. The rotors consist of helical lobes affixed to a shaft. One rotor is referred to as the male rotor and will usually consist of four lobes. The other rotor is referred to as the female rotor and consists of flutes that match the curvature of the male lobes. Female rotors typically have six valleys. For every revolution of the male rotor, the female rotor only turns through 240 degrees of rotation. Since the male rotor is the driven shaft, it is commonly referred to as four compression cycles per rotation (Smith, 2012).

The suction gas becomes trapped between two helically shaped cylinders created by the rotor screw threads and the casing as the threads rotate away from the open suction port. The total displacement is the volume at suction per thread times the number of lobes on the driving rotor. The male rotor lobe will start to enter the trapped gas in the female rotor flute on the bottom of the compressor at the suction end, creating the back edge of the trapped gas pocket. Further rotation will reduce the trapped volume and compress the trapped gas. The screw compressor has no valves, the discharge port location determines when compression is over. The volume of gas remaining in the trapped pocket at the discharge port opening is defined as the discharge volume. The gas then flows out through this port at approximately constant pressure (Stosic, 2004).

The majority of screw compressors designed today use oil injection into the compression area for lubrication, sealing of leakage paths, and cooling. The quantities of injected oil are approximately 10 to 20 gal/min per 100 hp (Pillis, 1999). The large oil quantities transfer most of the heat of compression to the oil and allows discharge temperatures to be low even at high compression ratios (Pillis, 1999). Oil injection performs useful functions in the screw compressor; however, since oil is introduced in other parts of the process, oil flooded screw compressors need oil separators. Since the majority of the heat of compression is transferred to the oil during compression, an oil cooling system is needed to remove this heat (Pillis, 1999).

Consequently, without the cooling of the gas by the oil during the compression process, the same temperature rise limitations as a centrifugal compressor apply to a dry screw compressor. The same oil is used for the lubrication of bearings and for the injection inside the machine (Almasi, 2015). Oil flooded screw compressors feature a pressurized reservoir and a gas/oil separator. The separator is a specialized component that usually includes proprietary internal design features to remove the oil entrained in the process gas stream prior to final process gas discharge from the package (API, 2010). The main objective of an oil flooded rotary screw compressor is to reduce the gas discharge temperature to a value less than 160°F or to limit the observed temperature rise to 100°F. This type of operation extends the volume and pressure capabilities while extending the service life of the compressor and its lubricant (Schell and Dreksler, 1976).

In one sense, the clearances in oil injected machines are easier to manage than in oil free machines as temperatures are normally kept within significantly lower limits. However, the absence of timing gears and the direct rotor to rotor drive does add more complexity to clearance analysis. Rotor contact is necessary for one rotor to drive the other; the objective is to precisely control where it is possible for contact to occur. The best practice for direct drive clearance design safeguards only rolling contact at the pitch radius of each rotor as offered by Stosic et al. (2005). Deviations from nominal design clearances, whether due to manufacturing and assembly tolerances or due to operational distortions, can cause a shift in the relative rotation between the male and female rotors which further distorts the interlobe clearance distribution and must be considered in clearance evaluation for direct drive, oil injected compressors (Sauls et al., 2007).

The advantages of an oil flooded screw compressor compared to other compressor types are summarized as follows (Almasi, 2015; Bloch & Geitner, 2012; Brown, 2005; Davidson & Bertele, 2000; API, 2010; Forsthoffer, 2011):

- considerably reduced sensitivity to gas composition and gas molecular weight change
- capability of accepting more liquid and entrainments than other compressors
- a lower cost
- a higher efficiency
- less maintenance
- good availability
- small size and a very compact package concept
- capable of providing up to 40 Bar(g) discharge pressure
- timing gears are not needed. The oil-flooded screw compressors are simpler and more robust.
- because of the oil injection, a higher compression ratio can be achieved without cooling.

Screw compressors are simple volumetric machines in which the moving parts all operate with rotational motion. This allows them to operate at higher speeds with less wear than other types of compressors available. As a result, they can be five times lighter than their reciprocating competitors of the same capacity and have up to ten times longer operating time between necessary overhauls. In addition, their internal geometry is

configured such that they have a negligible clearance volume, and leakage paths that decrease in size as compression proceeds. Thus, provided that the running clearances between the rotors and their housing are small, they can maintain high volumetric and adiabatic efficiencies over a large range of operating pressures and flows. Specialized machine tools enable the most complex rotor shapes to be manufactured with tolerances of 5 μm or less at an economical cost (Stosic, 2004).

The following is a list of oil flooded screw compressor features (Smith, 2012).

- Oil is injected into the gas stream for lubricating, cooling, and sealing.
- The internal clearances between both the rotors themselves and between the rotors and case are larger because the oil forms a seal.
- The operating speeds are normally lower because the compressors are more efficient due to less blow-by.
- The pressure ratios and discharge pressures are considerably higher than the dry screw compressors.
- Power consumption is typically greater than dry compressors due to the large quantity of oil moving through the system.

Vibration Analysis

Bearing engineers normally use fatigue as the failure mode with the assumption that the bearings are properly installed, operated and maintained as intended. Today, due to advancements in manufacturing technology and materials, bearing fatigue life is no longer the limiting factor and is responsible for less than 3% of failures in service. Unfortunately, bearings fail prematurely while in service due to contamination, poor lubrication, temperature extremes, poor fitment, mass unbalance and misalignment. All these factors cause an increase in bearing vibration. As a result, condition monitoring has been used for many years to detect degrading bearings before they catastrophically fail, resulting in associated downtime costs or significant damage to other parts of the machine (Lacey, 2007).

Vibration analysis is typically recognized as the best method for monitoring bearing condition. It is very effective with antifriction bearings, providing an indication of bearing deterioration in the early stages (Pillis, 1999). Defects in the rolling element bearings create a series of impacts which repeat periodically at a rate known as bearing defect frequencies (Saruhan et al., 2014). Vibration monitoring is now an established part of most planned maintenance regimes and relies on the known predictable vibration signatures which rolling bearings generate as the rolling surfaces degrade. However, in most applications, bearing vibration cannot be measured directly as the bearing vibration signature is modified by the machine structure. Trend analysis requires plotting the vibration level as a function of time in order to predict when the machine needs to be taken out of service for repair (Lacey, 2007).

One of the milestones of modern era vibration analysis was the publication in 1939 by T.C. Rathbone titled "Vibration Tolerance" in *Power Plant Engineering*. The paper included a severity chart to provide guidelines for judging the condition of rotating machinery based on its vibration level (Mitchell, 1999). Vibration analysis is a fundamental tool for condition monitoring that is performed using advanced electronic components such as transducers, computers and software. The two main components of vibration analysis are first separation of individual component signals and noise minimization, second is to find the defective components. In vibration monitoring, the widely used techniques are time domain analysis, frequency domain analysis and time-frequency domain analysis for determining fault and critical operation condition (Kiran Kumar et al., 2018).

The overall vibration level is the simplest way of measuring vibration and usually consists of measuring the root mean square (RMS) vibration of the bearing housing or other point on the compressor with the transducer located as close as possible to the bearing. This method involves measuring the vibration frequency over a wide range, for example 10-1,000 Hz or 10-10,000 Hz. The measurements are trended over time and compared with known levels of vibration allowing alarm level development to indicate a change in the machine operating condition. Alternatively, measurements can be compared with general industry standards. Although this method represents a quick and low-cost method of vibration monitoring, it is less sensitive to incipient defects (i.e. detects defects in the advanced condition) and has a limited diagnostic capability. In addition, it is easily influenced by other sources of vibration, such as unbalance, misalignment, looseness, electromagnetic vibration etc. (Lacey, 2007).

Oil Analysis

The basic role of lubrication is to reduce friction, which prevents the wear of material surfaces. As a result, it is necessary to monitor changes in lubricant performances, which determines a timely change of lubricant, thus prolonging its service life and preventing any major failures or damage to the system. As the contact element of the tribomechanical system, lubricant is a carrier of information about the status of the whole system from the aspect of tribological and other ageing processes. Oil analysis, based on a well-defined program,

is a very effective method for monitoring the state of technical systems, which ensures early warning signals of potential problems that could lead to failure and break down of technical systems (Sreten, 2012).

Using oil analysis for compressor oils has several benefits: reduction of unscheduled downtime, improvement of reliability, in organizing effectiveness of maintenance schedules, life extension, optimization of oil change intervals and reduction of cost of maintenance. Data acquisition is extremely difficult on equipment condition for parts, which cannot be observed due to their position. In these cases, oil analysis enables a continuous equipment condition monitoring and a timely response in order to prevent undesirable prolonged halts. The wear mechanism of a lubrication system consists of contact surface wear and lubricant consumption. If there is contact surface wear, then wear particles are present. Regardless of the availability of numerous methods for diagnosing the physicochemical changes of lubricants, in order to create an accurate picture of the condition of lubricants from the system, it is necessary to obtain a representative sample and therefore extremely important to obtain the sample in a proper way (Sreten, 2012).

Every sample needs to be accompanied by substantial documentation containing all relevant data, such as user name, lubricant name, sample label, date of sampling, date of sample delivery, type of device, lubricant quantity in the system, oil change date, refill data, number of operating hours, operating temperature, reasons for sample and any other information that could be of use for better understanding of the problem in question and the final interpretation of the obtained analysis results (Sreten, 2012). Factors such as adding or changing oil, filter changes and sampling techniques can distort the results. Standardized analytical methods to determine the typical condition monitoring parameters associated with lubricant quality have been established by the American Society for Testing and Materials (ASTM). The following tests are most frequently used in condition monitoring (Sreten, 2012):

- Spectrometric Analysis (wear metals)
- Analytical Ferrography
- Rotrode Filter Spectroscopy
- Infrared Analysis
- Viscosity
- Acid Number
- Base Number
- Karl Fischer (water)
- Particle Count (contamination code)

Oil analysis is a critical component of any compressor maintenance program. It is important to monitor for water content (Karl Fischer test) and viscosity change over time, which indicate oil breakdown or dilution. Excessive amounts of water can damage compressors if permitted to remain in the system. Wear metals analysis may detect some problems, but usually indicates problems rather late in the failure cycle. The quality of the lubricating oil is easily affected by temperature, moisture, contaminants, etc. Once the lubricating oil is polluted by water or solid particles, its lubricating property will deteriorate, which may lead to the abnormal wear of bearings and even burnt bearings. Erosion will also occur on the surface of a bearing if the bearing works in lubricating oil with an overly high moisture content for a long period of time.

In the lubrication analysis field, condition monitoring is generally used to describe analyses of in-service lubricants performed to provide an indication of the quality of a particular fluid to operate in its designed function. These analyses normally include measurements of oil viscosity, wear metals, particle count, acid number, base number, water, soot, nitration, sulfation, glycol contamination, oxidation, additive depletion, or gasoline contamination, etc. Such information can be associated with engine, machinery, and component failures and ensures that lubricants are changed only when required, customarily when a critical parameter is out of specification. In compressor mechanical systems, wear metals and acid number are crucial, especially in relation to bearing wear and corrosion (Van De Voort and Sedman, 2006).

The purpose of lubrication oil condition monitoring is to decide whether the oil has deteriorated to the point that it no longer fulfills its protective function and to offer early warning of the possibility of total failure. As stated by Sharman and Gandhi (2008), the key function of lubrication oil is to create a continuous film between surfaces in relative motion to decrease friction and eliminate wear, and thereby, eliminate seizure of the contacting parts. The secondary function is to cool the moving parts, protect metal surfaces from corrosion, flush away or eliminate ingress of contaminants and keep the mating component free of deposits.

The parameters that describe the oil performance or level of degradation are referred to as performance parameters. These parameters typically consist of viscosity, water content, acid number, base number, particle counting, pH value and so forth (Zhu et al., 2013). Oil analysis is the control tool used to grade the effectiveness of machine lubrication practices and activities. The progressions to failure of many lubricated components follow degraded lubricant health and contaminated sumps. The predominant threat to long term performance is surface wear. Wear is caused by a handful of reoccurring problems. One of the most common applications for

oil analysis is machine condition assessment by wear debris measurement. This is commonly performed through spectrographic analysis, which reports metals in parts per million. The proper use of oil analysis can easily result in extended oil change intervals by a factor of three or more (Johnson and Spurlock, 2009).

Wear metal monitoring originated in the 1960s to complement lube quality and contamination monitoring. This approach began by U.S. commercial railroads in the late 1940s, but was typically restricted to this single application for over a decade because analyses were performed with bench testing by chemists, one metal at a time (Poley, 2007). According to Karanoviet al. (2018), there are four primary sources for solid particle contamination: contaminated new oil, built-in contamination, contamination ingress and internally generated contamination. Particle counting is normally thought of as a tool for determining overall cleanliness and contamination in used oil. However, particle count values can be also used to assist in the detection of wear debris in a sump. The particle count test is used as a primary test for the identification of particle contamination. Atmospheric particles accumulate in the oil through normal thermal cycles, through routine topup activities and from containers used to transport and store the lubricants. A correlation exists between the concentration of atmospheric particles (much of which are harder than the machine steel surfaces) and component wear. The resulting wear creates additional wear and causes oil health to decline, creating a self-perpetuating escalation (Johnson and Spurlock, 2009).

The number of solid particles over different sizes are counted, which can help in evaluating the contamination level of lubricating oil according to the ISO 4406 standard (Xu et al., 2016). The purpose of the ISO 4406 contamination code is to simplify the reporting of particle count data by converting the numbers of particles into broad classes or codes, where an increase in one code is generally a doubling of the contamination level. The code for contamination levels using automatic particle counters comprises three scale numbers that permit the differentiation of the dimension and the distribution of the particles. The first scale number indicates the number of particles equal to or larger than 4 μm per milliliter of fluid. The second scale number indicates the number of particles equal to or larger than 6 μm per milliliter of fluid. The third scale number indicates the number of particles equal to or larger than 14 μm per milliliter of fluid (ISO, 2017).

II. METHODOLOGY

This investigation focuses on an instrument air compressor in an oil and gas plant. The unit is a 300 HP motor operating at 1,787 RPM direct coupled to an oil flooded screw compressor. There are six lobes on the driven male rotor and four lobes on the female rotor. There are back to back anti friction tapered roller thrust bearings on the non-drive end (NDE) of the rotors and single anti friction roller bearings on the drive end (DE) of the rotors. The compressor has an ISO 68 viscosity grade oil with dual oil filters which allow for replacement based on differential pressure without shutting down the unit. The objective of the case study was to determine which condition monitoring technology, vibration analysis or oil analysis, is the most effective at predicting a fault in screw compressor operating condition.

Periodic route-based vibration data is collected on a monthly basis by a ISO 18436 Category II certified analyst. Data is collected on the DE and NDE of the compressor in the horizontal, vertical and axial measurement planes. Spectral and time waveform analysis are performed along with overall trending to determine the operating condition of the compressor. The overall values are collected as velocity units of measurement (mm/sec RMS) and based on an Fmax of 2,000 Hz and 12,800 lines of resolution. The API 619 overall vibration limits for oil flooded screw compressors with rolling element bearings measured on a machine case is < 8.0 mm/sec RMS. The vibration analysis results dictate any corrective maintenance activities that may be required. Typical faults identified include misalignment, bearing defects, soft foot, etc.

Periodic oil samples are collected on a monthly basis downstream of the lube oil pump and upstream of the filter. Only trained personnel familiar with the proper sampling methods collect the samples to ensure continuity between samples. The samples are transported to a third-party laboratory with ISO 17025 accreditation to perform oil analysis. The samples are analyzed for viscosity, acid number, water content, wear metals, additive metals and particle count. The acceptable ISO 4406 contamination code is 18/16/13 based on industry recognized and generally accepted good engineering practices for compressor oil. The analysis results dictate maintenance activities that may be required such as oil changes and bearing inspections.

III. RESULTS

A new oil flooded screw compressor was installed and condition monitoring, both vibration analysis and oil analysis, were implemented immediately upon commissioning. The oil analysis particle count (4 μm and 6 μm) drastically increased after 70 days of operation and the oil was changed after 96 days of operation based on the oil analysis results. The ISO 4406 contamination code reached 27/26/22. The vibration analysis trended steady based on overall velocity readings collected on the DE and NDE compressor bearings at all six measurement planes. See figures 2 thru 4 for graphs of overall vibration and particle count over time. At the next monthly condition monitoring data collection, 136 days of operation, the oil analysis revealed the particle count

had already begun to increase. The vibration levels eventually began to increase after 148 days of operation. The overall vibration levels reached 15.9 mm/sec RMS at the NDE bearings in both the horizontal and vertical measurement planes. The compressor failed after 192 days of operation. The point of failure was a NDE bearing with a broken cage, spalling on the rollers and fretting on the outer race. A root cause failure investigation later determined the root cause to be operating outside of the designed operating conditions due to improper process valve position. See figures 5 thru 7 for pictures of the failed bearings. The rotors showed signs of contact which presumably occurred after the bearings failed and no longer maintained the position of the rotors. See figure 8 for a picture of the rotors.

IV. CONCLUSION

The oil analysis indicated an increased particle count indicating a fault after 70 days of operation. The vibration analysis measured as overall velocity detected a fault after 148 day of operation. The oil analysis condition monitoring technology was able to detect the bearing fault 53% (78 days) earlier than the overall vibration analysis. This is counterintuitive based on the widespread industry acceptance of vibration analysis as the superior condition monitoring technology. Vibration analysis is superior to oil analysis in its ability to detail the specific source of pending failure (inner race, outer race, ball spin, ball pass, cage). However, the less specific alert provided by oil analysis was received much earlier.

It can be deduced that the wear metals collected downstream of the pump and upstream of the filter must be originating from the bearings. The only wear metals found in the oil analysis was iron at 21 ppm which is indicative of a bearing fault. The specific bearing failure mode (inner race, outer race, ball spin, ball pass or cage) is irrelevant as the bearings will need to be replaced regardless of the fault. This should encourage condition monitoring practitioners to place more importance on the results of their oil analysis. In comparison with vibration condition monitoring technologies, lubrication oil condition monitoring provides approximately 2 times earlier warnings for machine malfunction and failure.

FIGURES

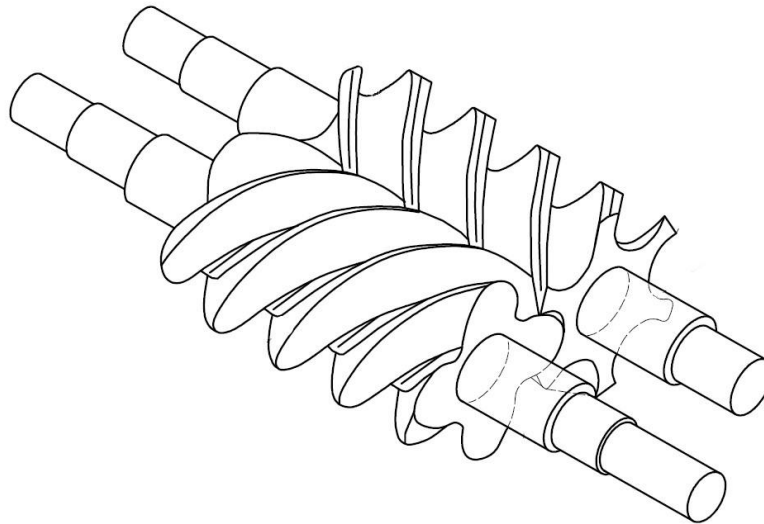


Figure 1 –Screw Compressor Rotors (API, 2010)

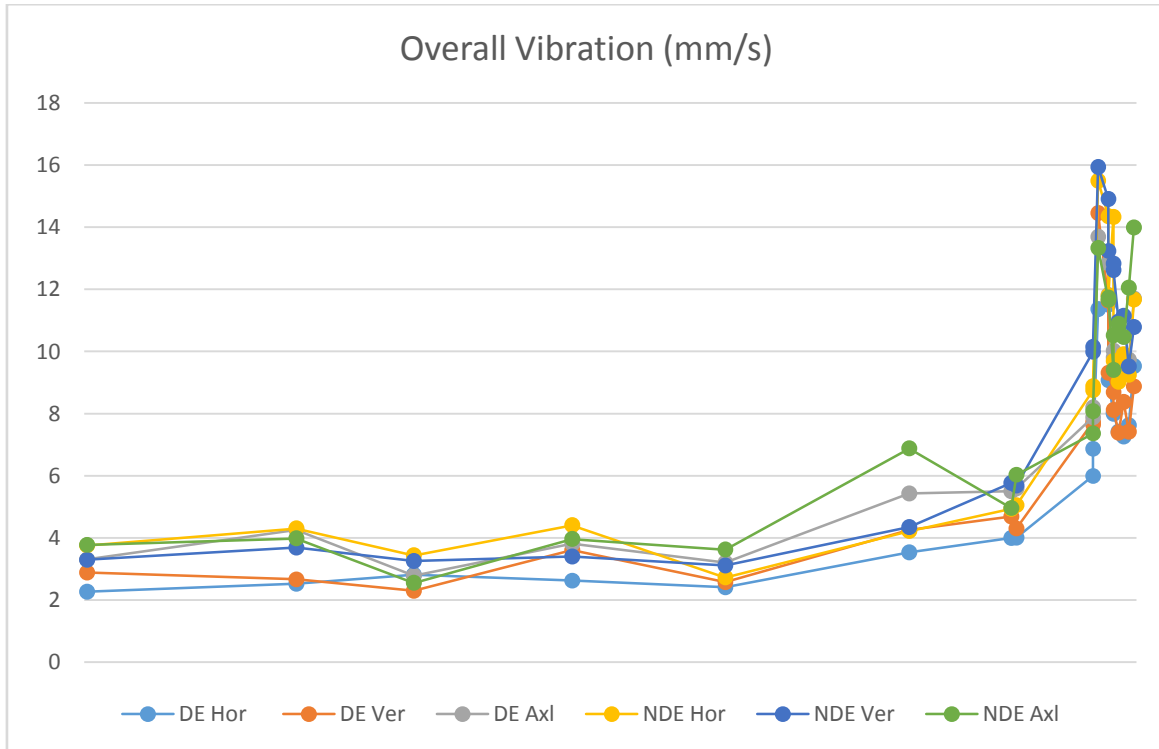


Figure 2 – Overall Vibration Over Time

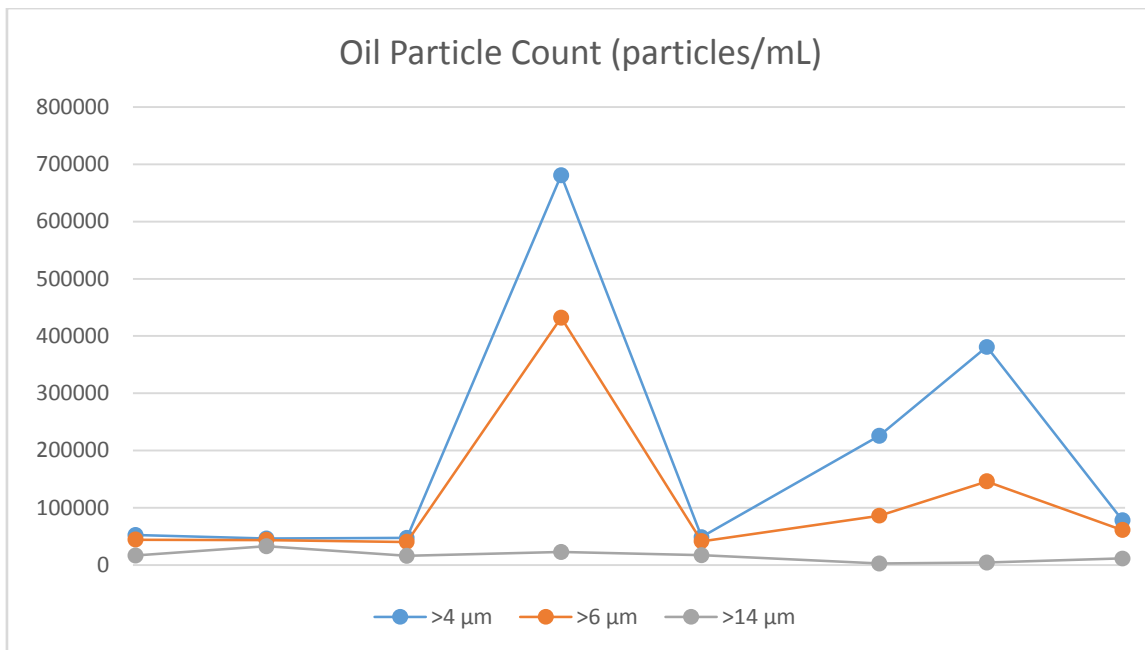


Figure 3 – Oil Particle Count Over Time

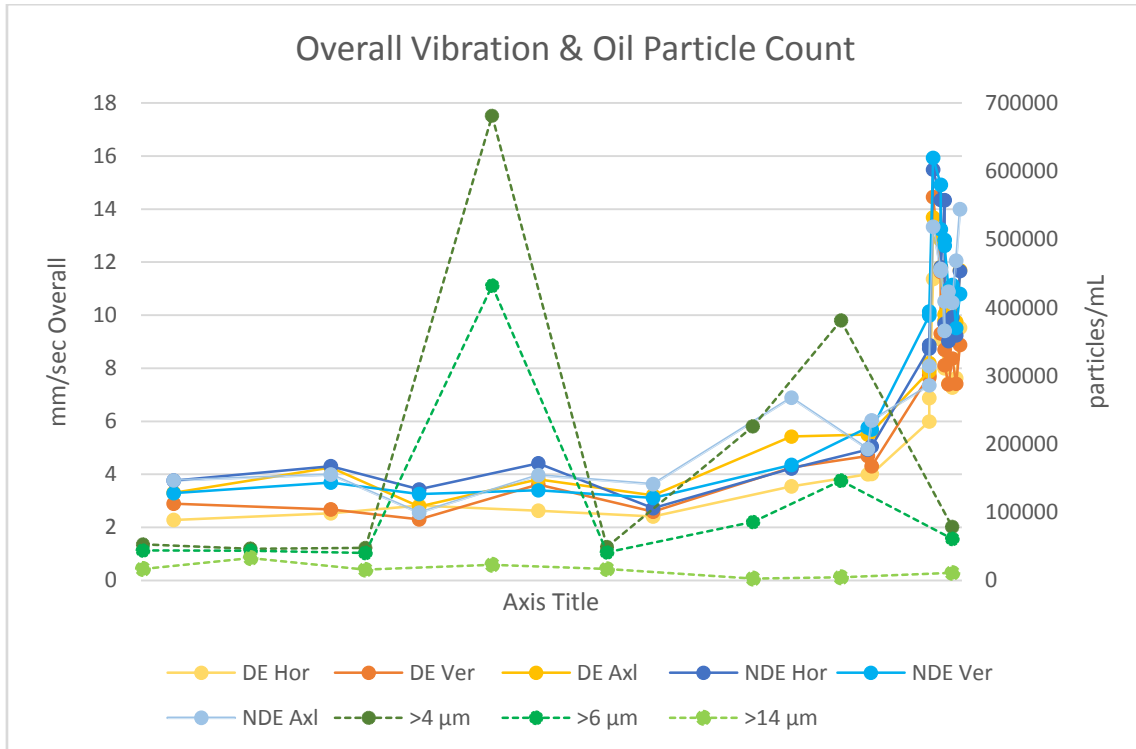


Figure 4 – Overall Vibration & Oil Particle Count Over Time



Figure 5 – DE Bearing



Figure 6 – NDE Bearing Cage



Figure 7 –NDE Bearing Outer Race



Figure 8 – Rotors

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